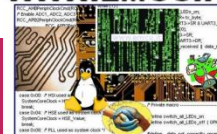


# **ST Microelectronics**

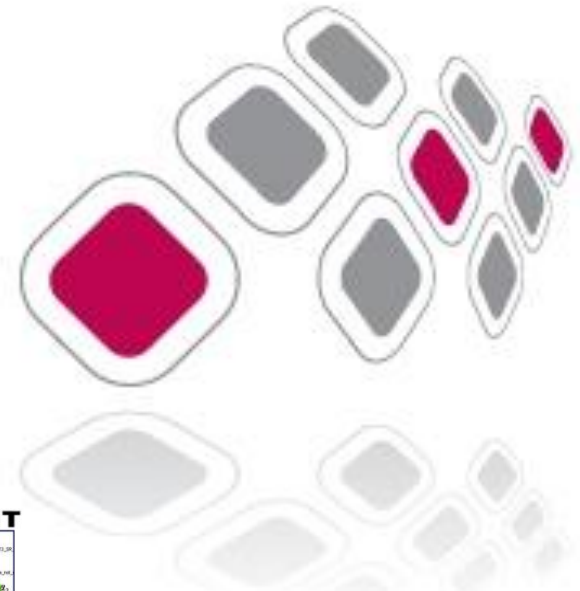


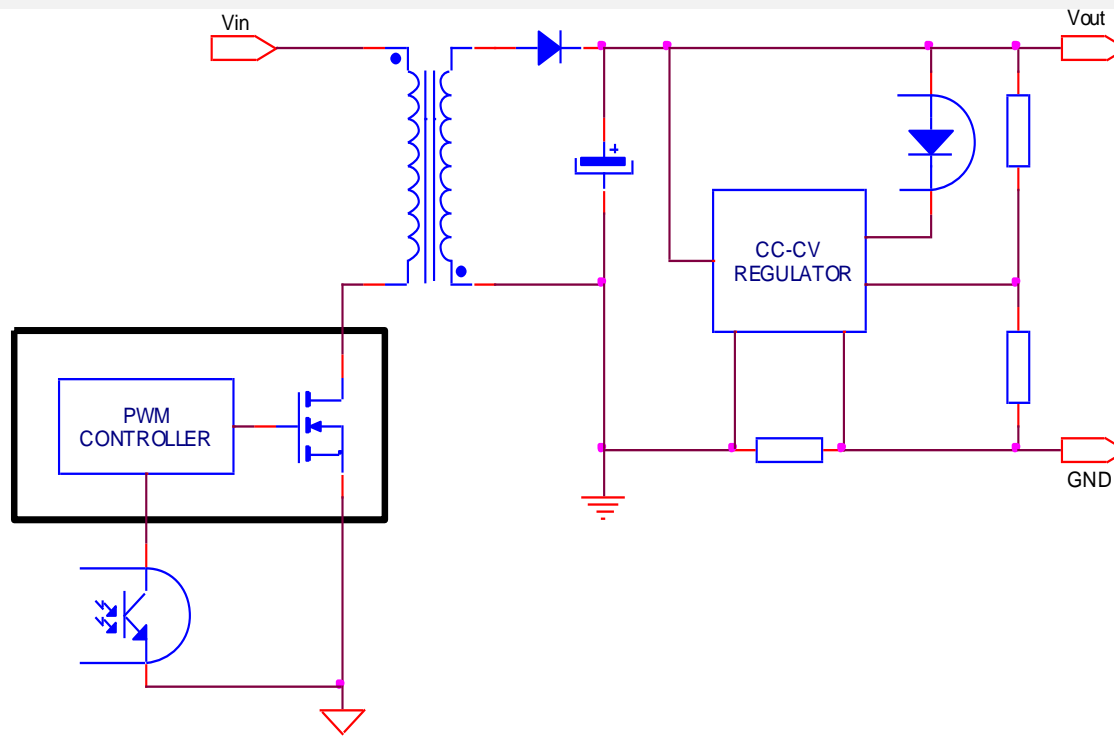


# Off-line All-Primary AC/DC converter

## ALTAIR05T-800

## ALTAIR04 - 900

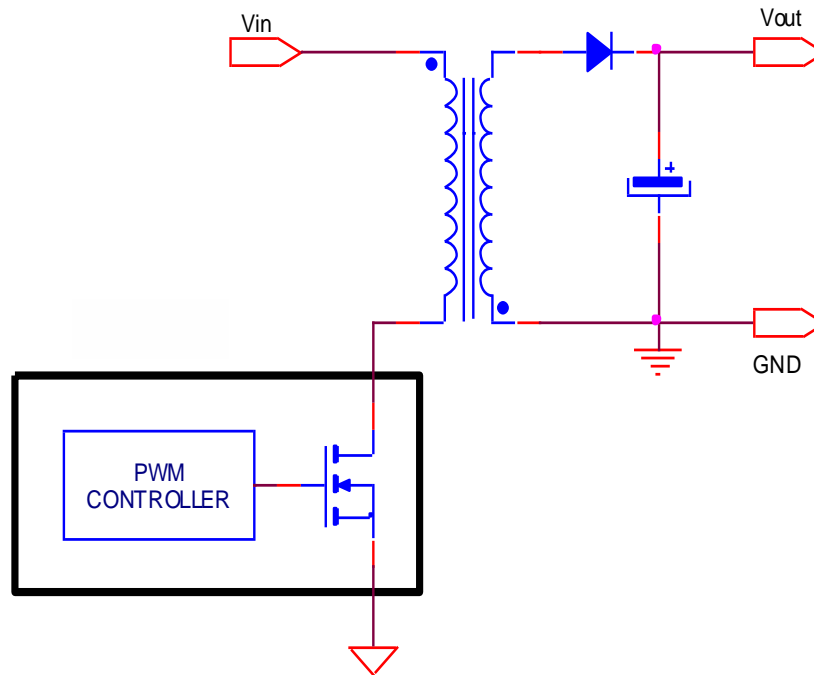




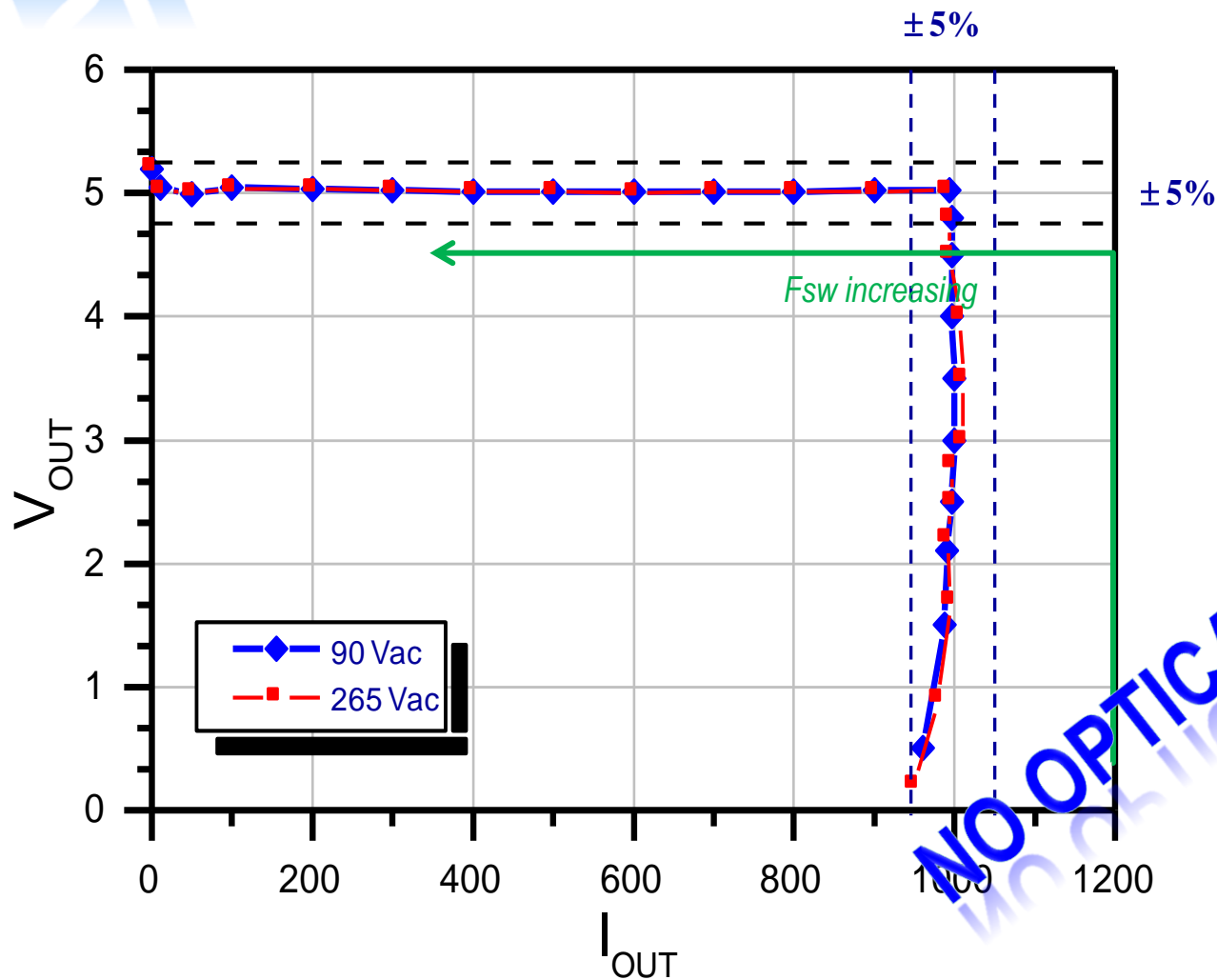
➤ Accurate CC-CV regulation

- Need dedicated CV-CC regulator
- Need secondary components and opto
- Power dissipation on sense resistor
- Expensive solution

# Proposed (CV-CC) application solution



- Control of output voltage and current entirely from primary side
- Benefit: Save all secondary regulation components (voltage reference, error amplifier(s), optocoupler, sense resistor)

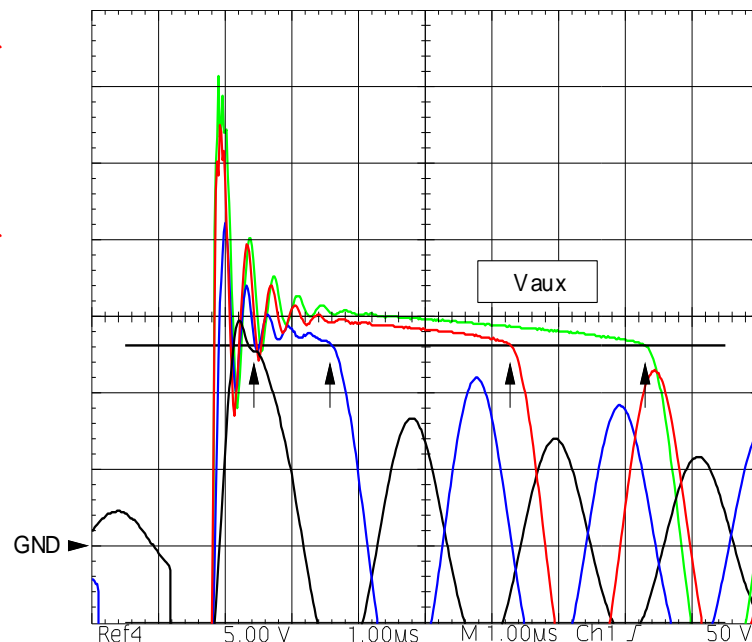
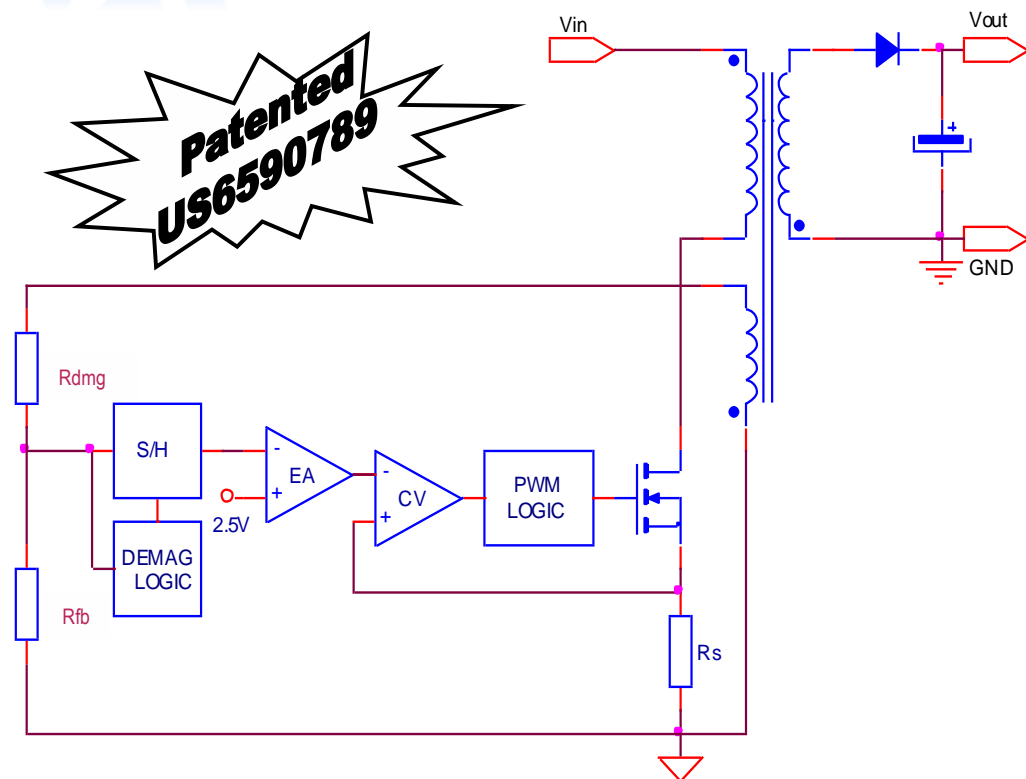


WWW.EMCU.IT



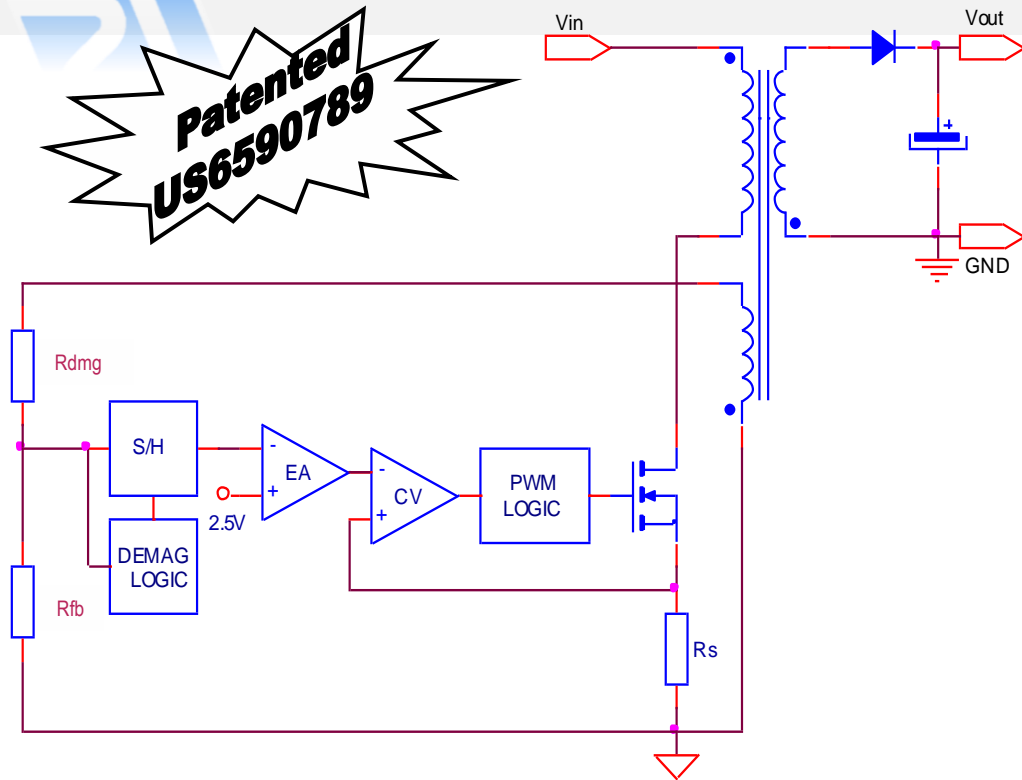
# Constant Voltage Mode

## Principle of operations

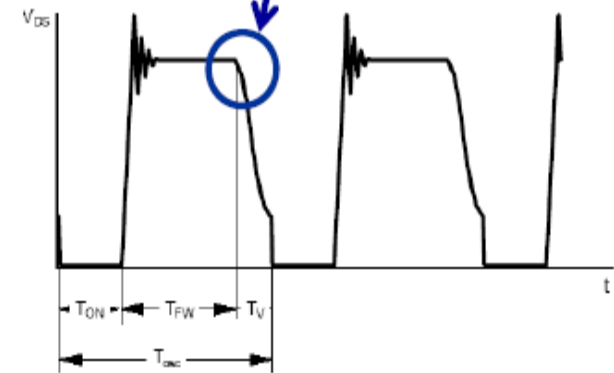


An accurate image of the output voltage can be obtained by sampling the voltage of the auxiliary winding right at the end of transformer's demagnetization. An ST proprietary technique to do the job.

**Patented**  
**US6590789**

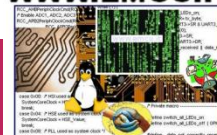


*DMG proportional to Vout  
(hold instant)*



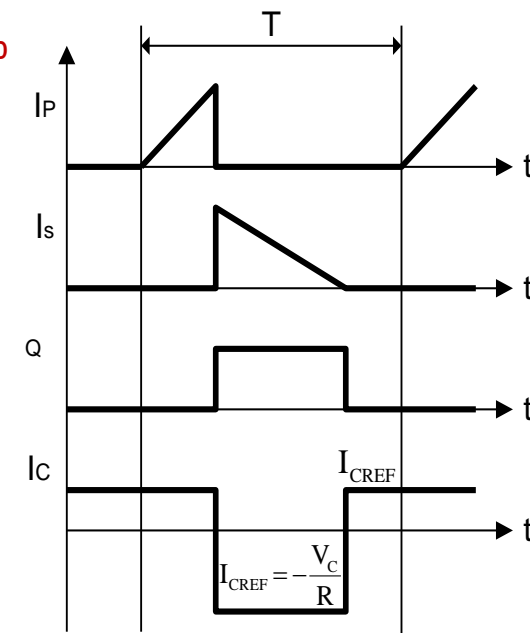
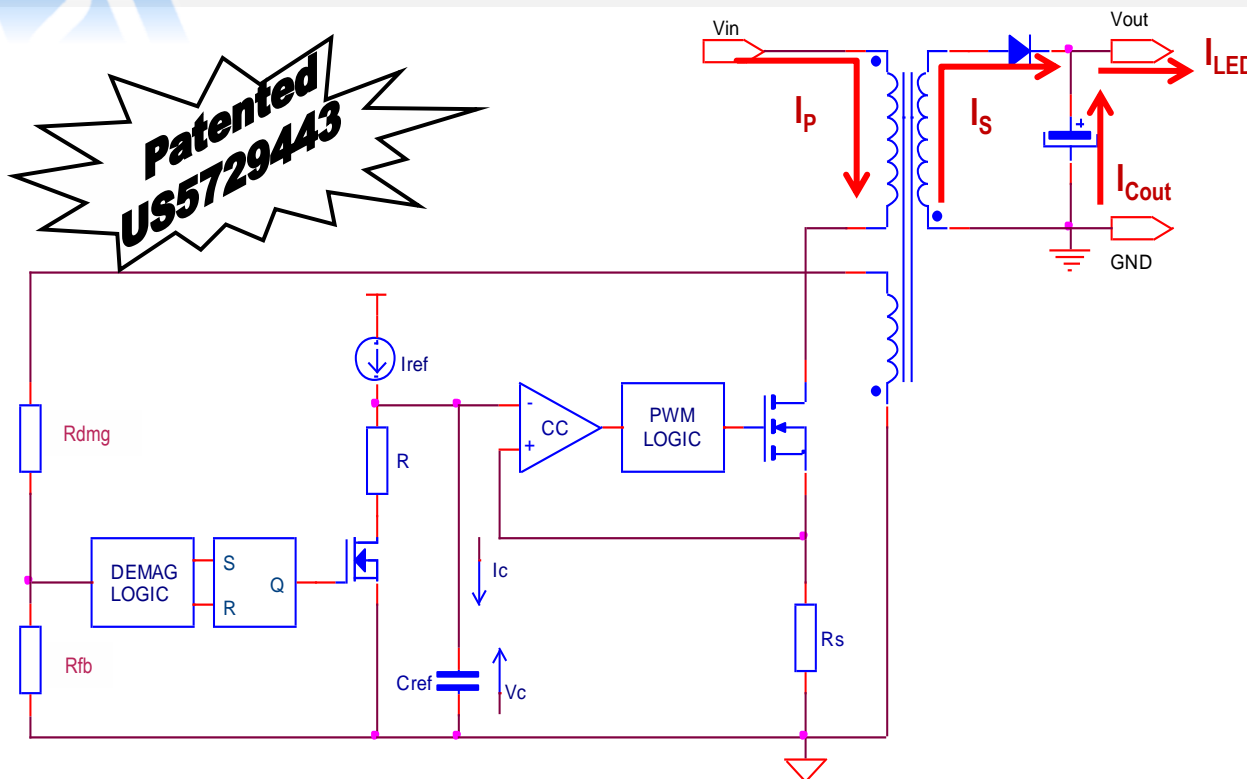
$$V_{DMG} = \frac{R_{FB}}{R_{FB} + R_{DMG}} * \frac{N_{aux}}{N_s} * V_{out}$$

An accurate image of the output voltage can be obtained by sampling the voltage of the auxiliary winding right at the end of transformer's demagnetization. An ST proprietary technique to do the job.





**Patented**  
**US5729443**



$$I_{OUT} = \frac{n \cdot I_P}{2} \cdot \left( \frac{T_{ONSEC}}{T} \right)$$

$$I_{REF} \cdot (T - T_{ONSEC}) + \left( I_{REF} - \frac{V_C}{R} \right) \cdot T_{ONSEC} = 0$$

$$I_P = \frac{V_C}{R_{SENSE}}$$

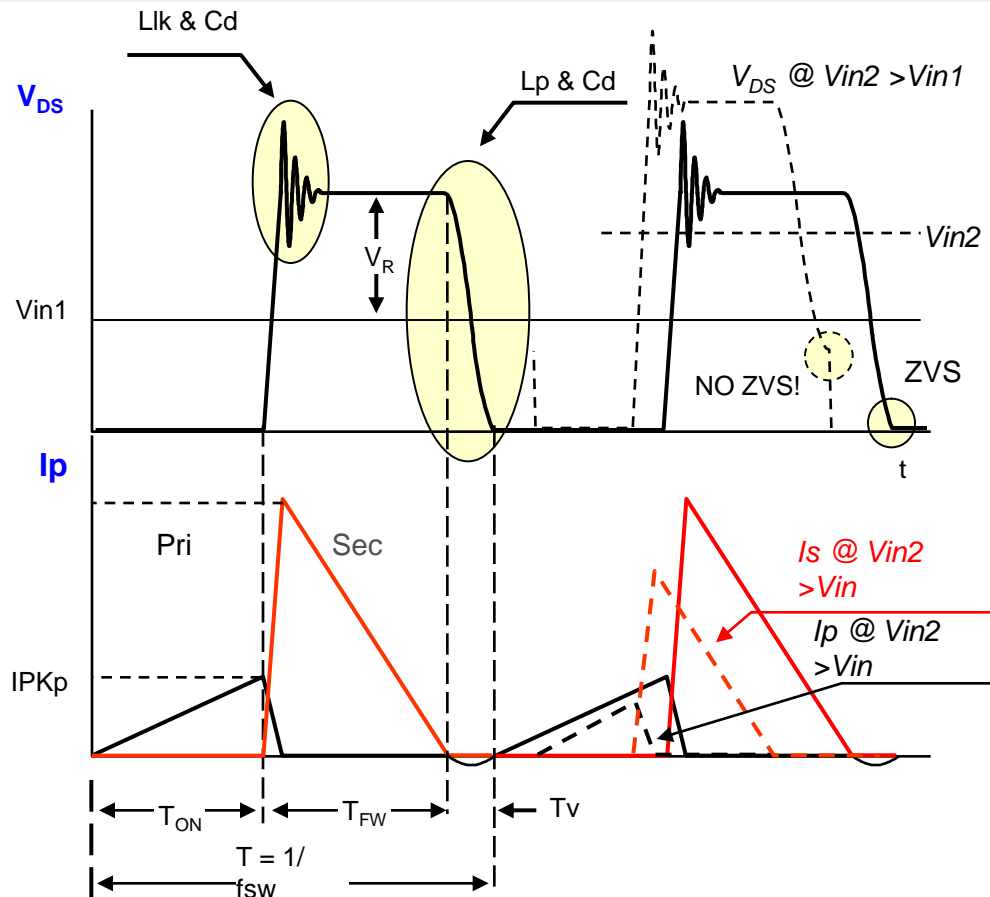
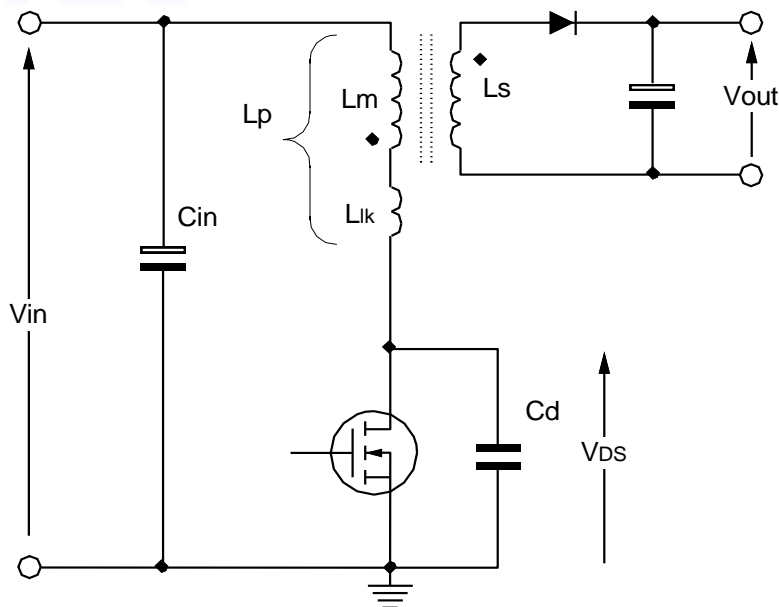
$$I_{OUT} = \frac{n}{2} \cdot \frac{R \cdot I_{REF}}{R_{SENSE}}$$

**WWW.EMCU.IT**



- ✓ Valid in DCM only
- ✓ Iout does not depend on either Vin, Vout or Fsw
- ✓ Cout net charge exchange is null





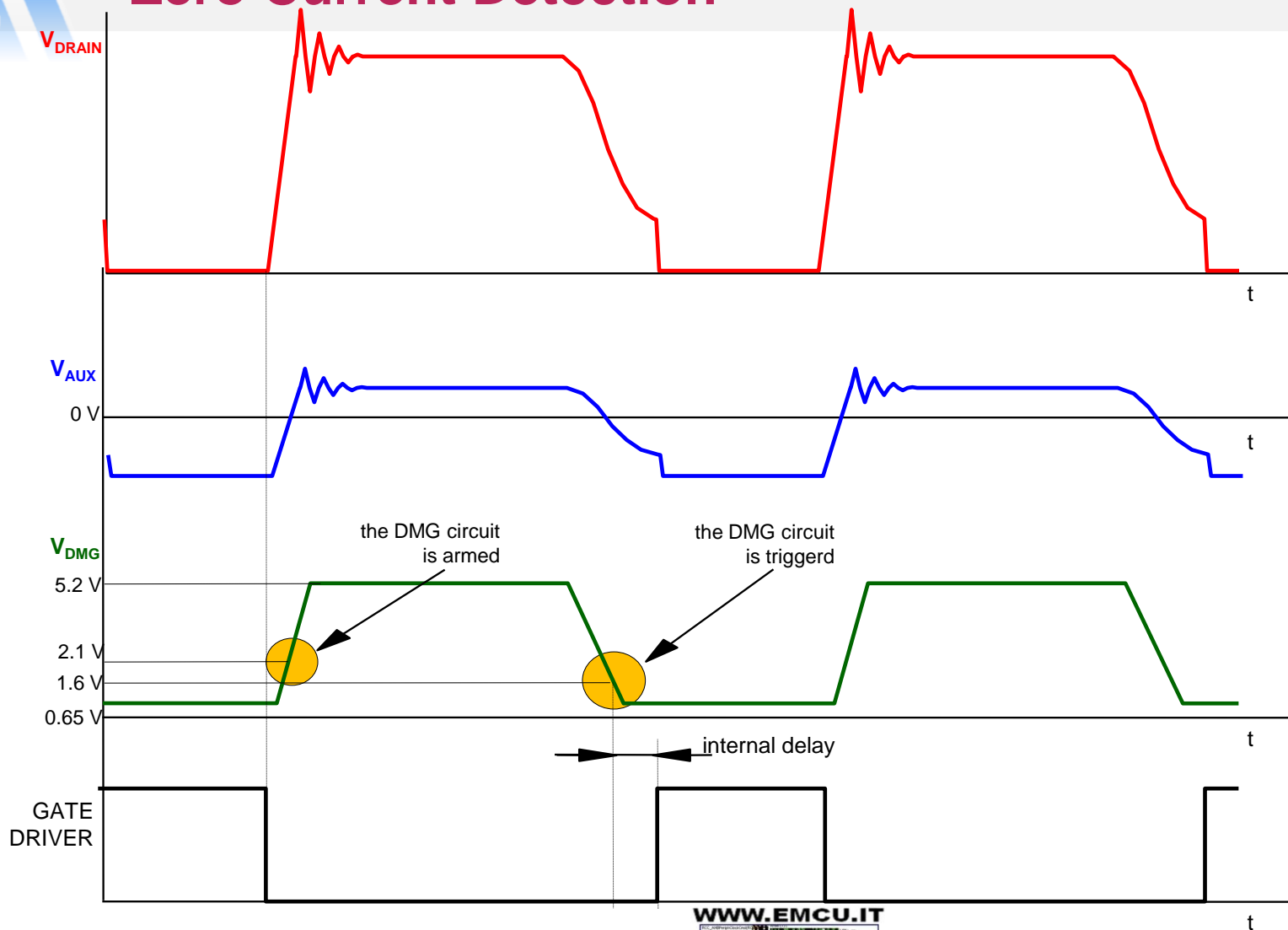
- ✓ Operation close to the boundary between CCM and DCM
- ✓ Zero Voltage / Zero Current Switching at turn-on achievable
- ✓ Less EMI
- ✓ Variable Frequency spreads spectrum

ZVS condition:  $V_{in} < V_R$



# QR Conversion

## Zero Current Detection

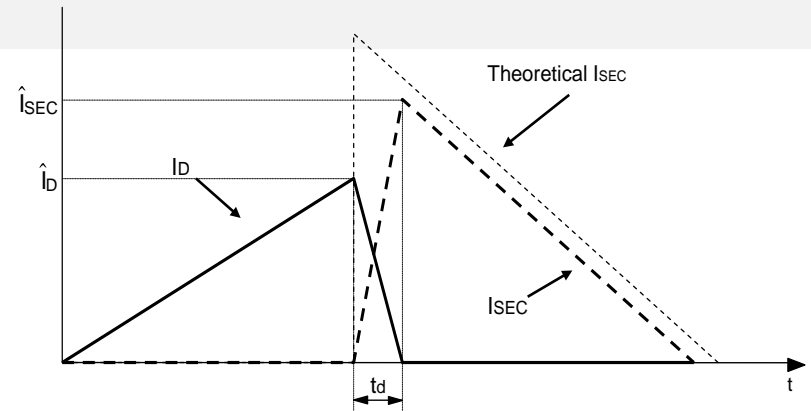
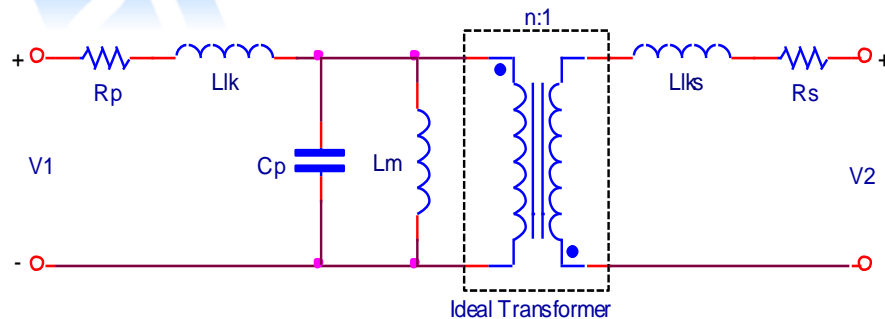


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# Constant Current Mode

## Transformer coupling



- ✓ The energy on the primary is transferred to the secondary side only once the parasitic capacitor  $C_p$  is charged to  $V_{cp} = -n V_{out}$ .
- ✓ The resulting transfer time delay causes the peak secondary current to be less than the theoretical one, resulting in an effective turn's ratio less than the theoretical one.

$$n_{REAL} = n \cdot \left[ 1 - \frac{L_{LK}}{L_P - L_{LK}} \cdot \frac{n \cdot V_{OUT}}{V_S - n \cdot V_{OUT}} \right]$$

- ✓ A leakage inductance of 3% can easily deliver an output current 10% lower than the one computed.
- ✓ All these parameters are generally repetitive in production and easily compensated.

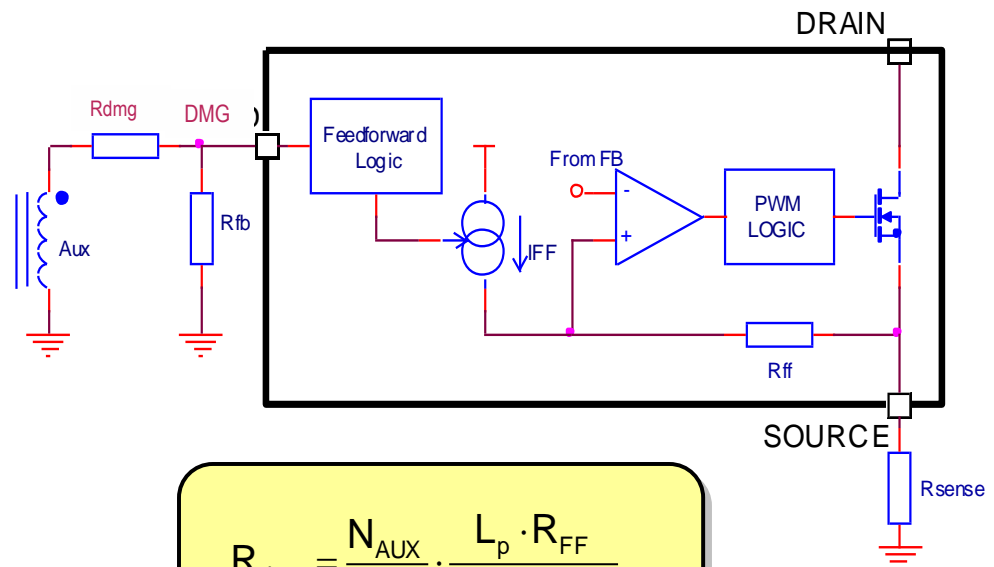
- ❑ The internal current comparator propagation delay ( $T_d$ ) switches off the MOSFET with a higher peak current than the foreseen.
- ❑ Current variation depends on input voltage

$$\Delta I_p = \frac{V_{IN} \cdot T_d}{L_p}$$

Feedforward compensation introduces a negative offset that is proportional to input voltage to compensate  $T_d$

$$V_{OFFSET} = I_{FF} \cdot R_{FF} = \frac{V_{IN}}{R_{dmg}} \cdot \frac{N_{AUX}}{N_{PRI}} \cdot R_{FF}$$

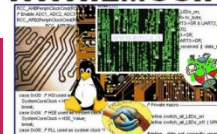
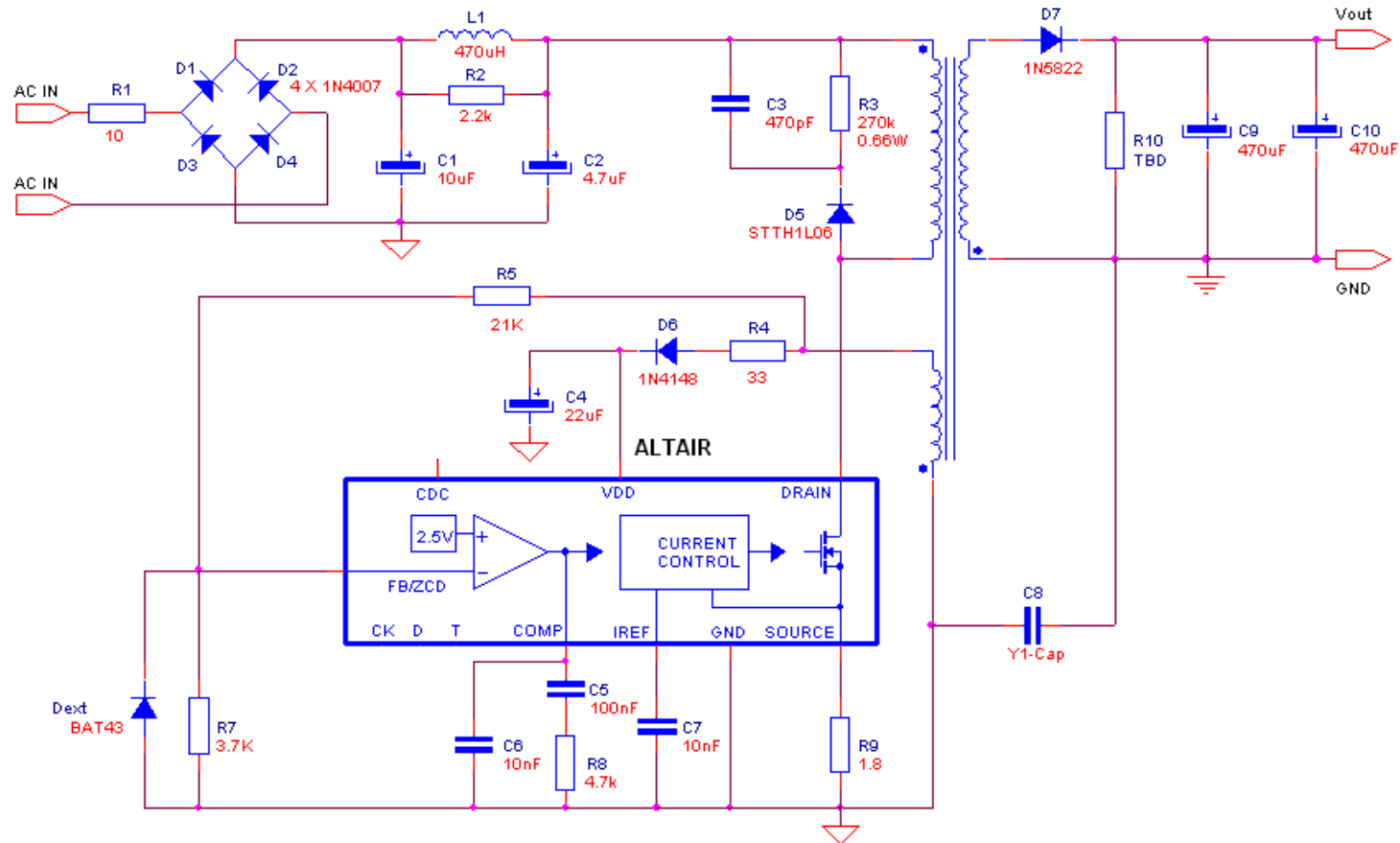
$$\frac{V_{IN} \cdot T_d}{L_p} \cdot R_{SENSE} = \frac{V_{IN} \cdot R_{FF}}{R_{dmg}} \cdot \frac{N_{AUX}}{N_{PRI}}$$



$$R_{dmg} = \frac{N_{AUX}}{N_{PRI}} \cdot \frac{L_p \cdot R_{FF}}{T_d \cdot R_{SENSE}}$$

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## Boards

### EVLALTAIR900-M1

(7.5W double output wide range for PLM)



### EVLALTAIR05T-5W

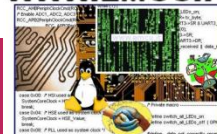
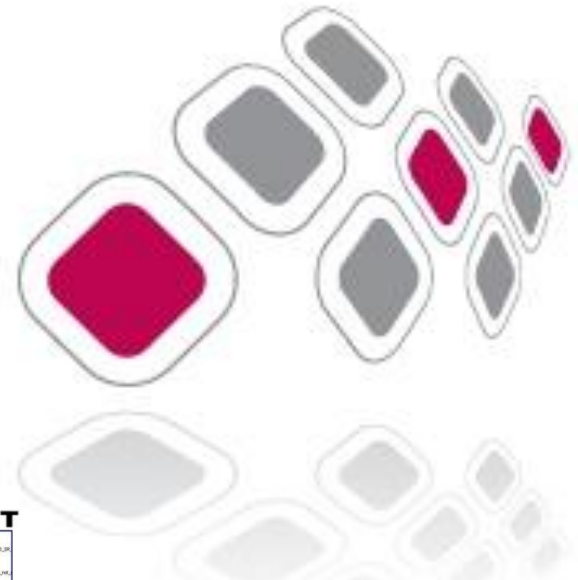
(5W - 5V Single output wide range )

- *Control of output voltage and current entirely from primary side*
- *Accuracy 5% the best in primary control*
- *Benefit: NO! secondary regulation components (voltage reference, error amplifier(s), optocoupler, sense resistor)*

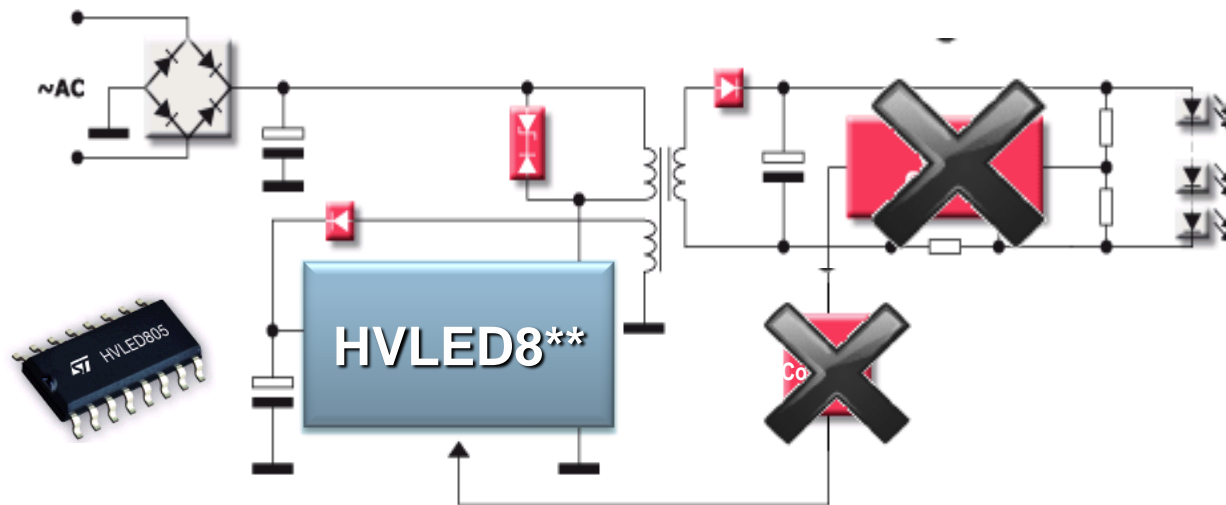


# HVLED family: the new off-line LED driver family

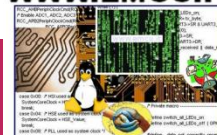
*Lighting the future*



- ▶ **HVLED8\*\* operates directly from the Mains voltage for ISOLATED AC-DC LED drivers**
  - requiring only minimum external parts
    - ✚ Controller and MOSFET in the same chip
  - performing primary LED current control
    - ✚ no need of secondary sensing (sense resistor and CC controller)



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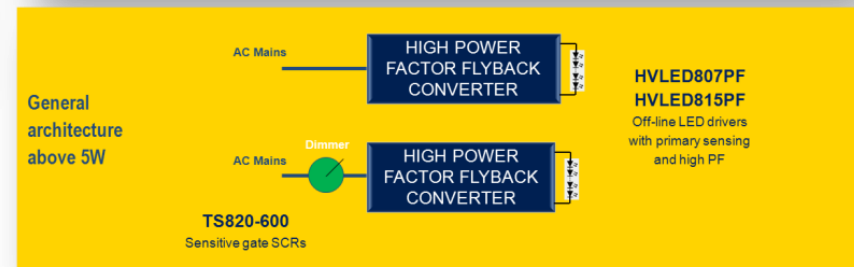
# General illumination HVLED family - products

## ► APPLICATIONS

- Retrofit of incandescent lamps
- AC Mains supplied spot lamps



Up to 15W



HVLED805



HVLED807PF



HVLED815PF



5W

7W

15W

Maximum output power for  $V_{IN} = 185 - 265V_{AC}$

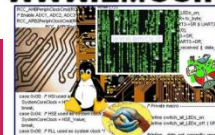


High PF > 5W  
>0.7 residential  
>0.9 commercial

platforms with variable number of LEDs in series

compliant with PF requirements

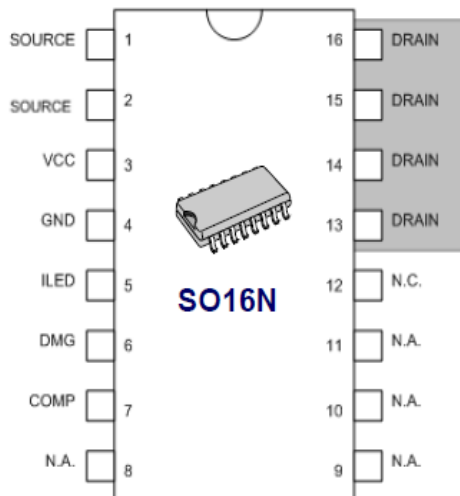
800V integrated mosfet (*state-of-the-art*) reduces application cost





# HVLEDxx pinout

## HVLED805

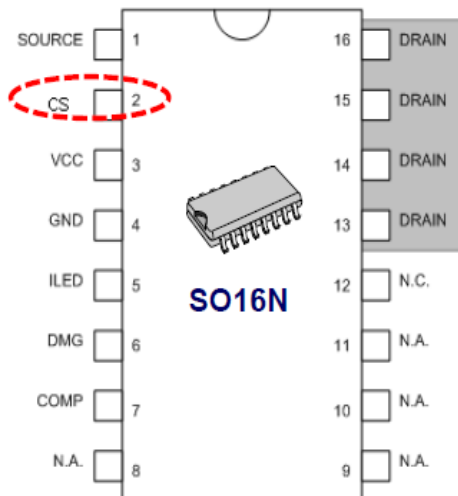


Rds\_ON: 11Ω (typ)

Tdelay (MOS OFF): 330ns (typ)

3-5 W

## HVLED807PF



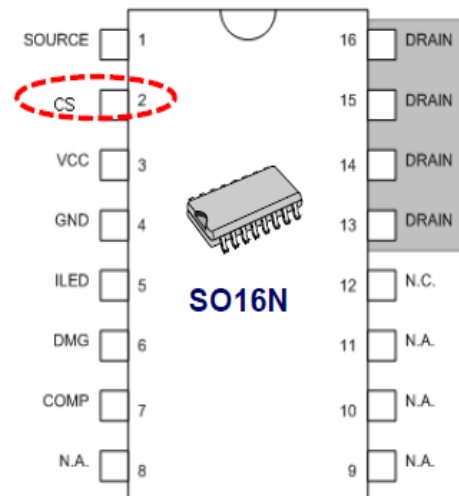
Rds\_ON: 11Ω (typ)

Tdelay (MOS OFF): 100ns (typ)

CS pin available - for high PF

5 ~7 W

## HVLED815PF



Rds\_ON: 6Ω (typ)

Tdelay (MOS OFF): 100ns (typ)

CS pin available - for high PF

Up to 15 W





# General illumination HVLED family - products

Internal 800 V avalanche rugged Power MOSFET and HV start-up

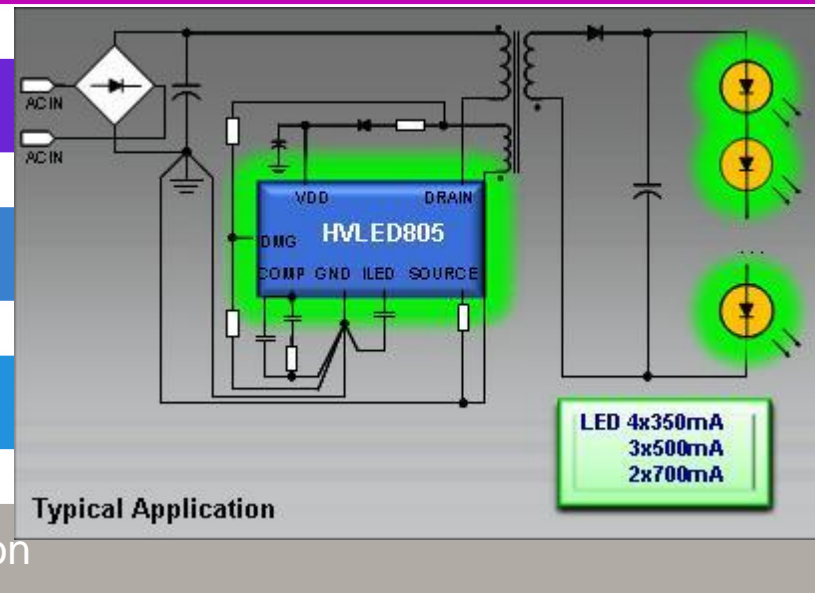
3% (HVLED807PF and HVLED815PF) or 5% (HVLED805) accuracy

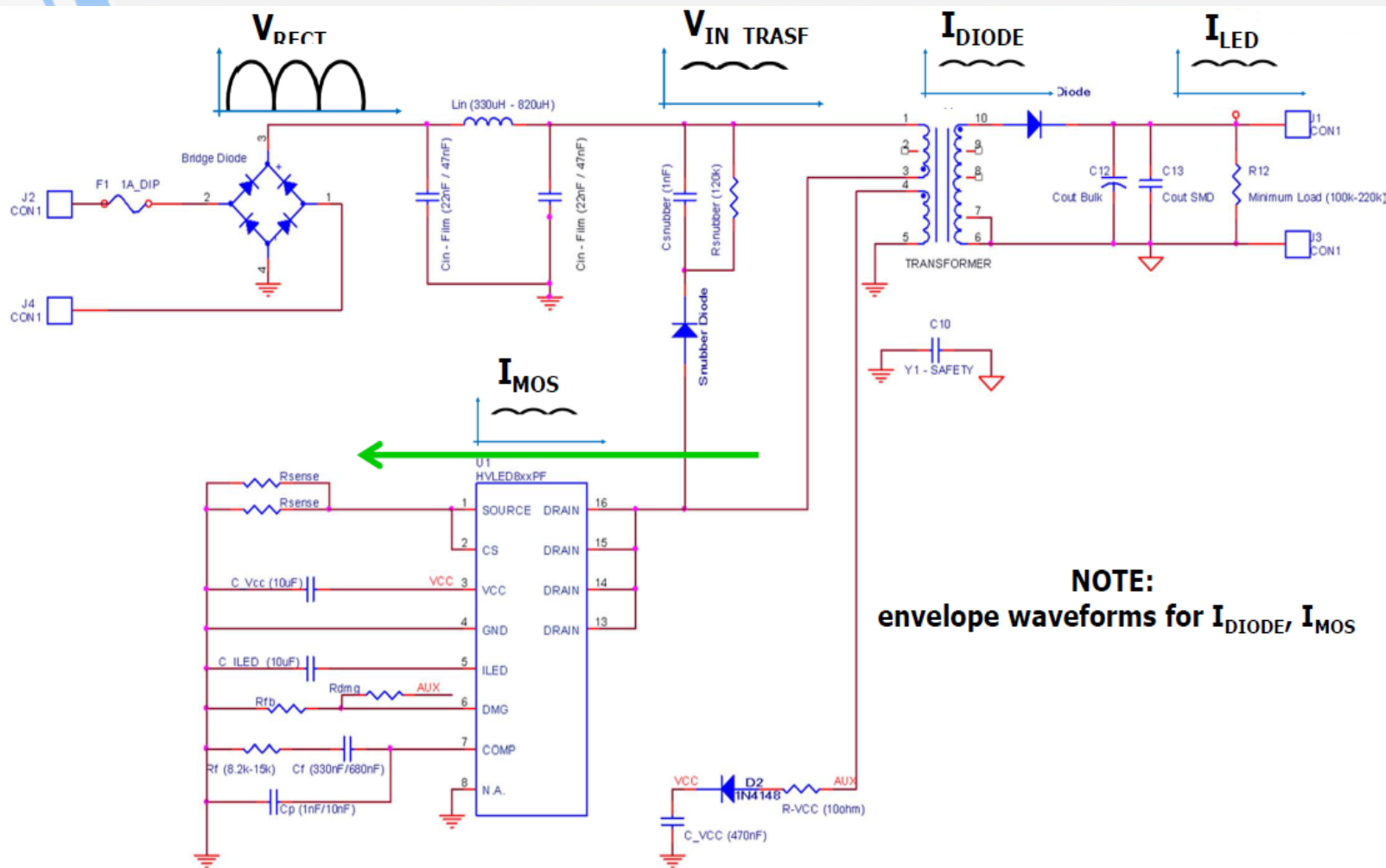
Primary Sensing Regulation

Quasi resonant operation mode

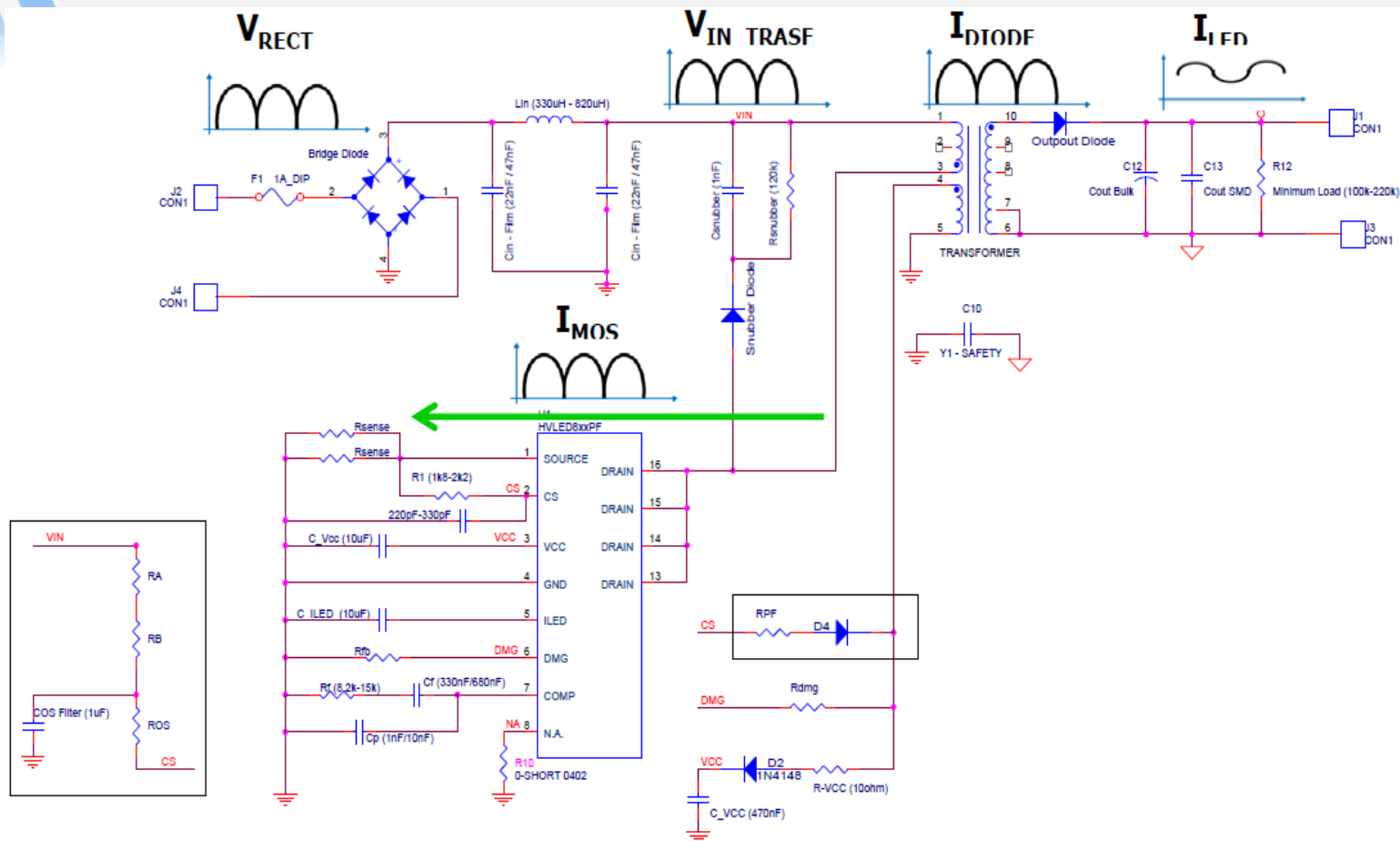
Automatic self supply

Open and short LED string protection



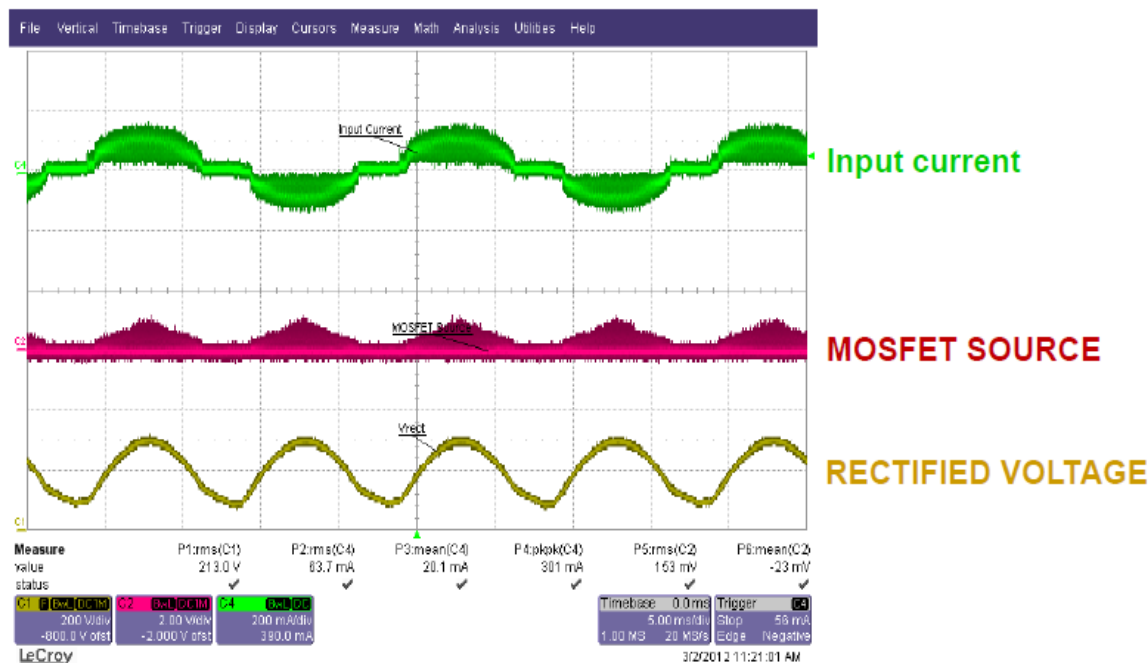


Standard schematic using HVLED805 (PF 0.5/0.6)



**High PF (>0.9) implementation using HVLED807PF/815PF**

PF=0.95; THD= 21%



CH1(green)=lin; CH2(purple)=MOS Source; CH1(yellow)=Vin\_rect

***“Input current” in phase with the input voltage***

Note: test results on 12W solution – 3-V/340 mA LED output



# General illumination

## HVLED family – tools 1/2

Up to 15W

### EVALHVLED815 (\*)

10.2 W LED power supply  
based on HVLED815PF  
HPF Flyback

NEW



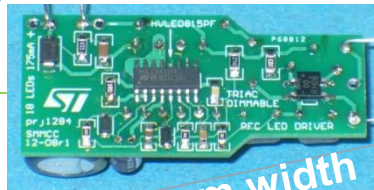
- Vin = 185-265 Vac
- Iled = 340mA
- Vout = 30V
- Power factor = 0.92
- Average efficiency 86%

AN draft (\*)

### STEVAL-ILL044V1 (\*), (\*\*)

9 W Triac dimmable  
LED power supply  
based on HVLED815PF  
HPF Flyback

NEW



- Vin = 90-132 Vac
- Iled = 175mA
- Voutmax = 56V
- Power factor >0.98
- Efficiency >86%
- Dimmable over 90V to 132V range
- Isolated version (\*\*)

AN4129  
AN4130

### STEVAL-ILD003V1 / V2

6W / 8W Home analog Light dimmer  
based on TS820-600



- Suitable for LED & CFL retrofit & incandescent lamps
- 230 V – 50 Hz Line (V1 version), 120 V – 60 Hz Line (V2 version)
- Leading edge-control
- Control with potentiometer
- Dimmable LED lamps:  
6W (V1 version), 8W (V2 version)
- Dimmable 14W CFL lamps

UM1512

UM1513

(\*) Available in Q4 2012

(\*\*) Not isolated version available STEVAL-ILL045V1





# General illumination

## HVLED family – tools <sup>2/2</sup>

Up to 15W

### EVALHVLED805

4.2 W LED power supply  
based on HVLED805  
Flyback



- $V_{in} = 185-230 \text{ Vac}$
- $I_{led} = 350\text{mA}$
- $V_{outmax} = 12\text{V}$
- Output current ripple < 10%
- Average efficiency > 70%

Data brief

### STEVAL – ILL037V1

3.2 W LED power supply  
based on HVLED805  
Flyback



- $V_{in} = 90-265 \text{ Vac}$
- $I_{led} = 200\text{mA}$
- $V_{outmax} = 16\text{V}$
- Efficiency = 85%

AN3360

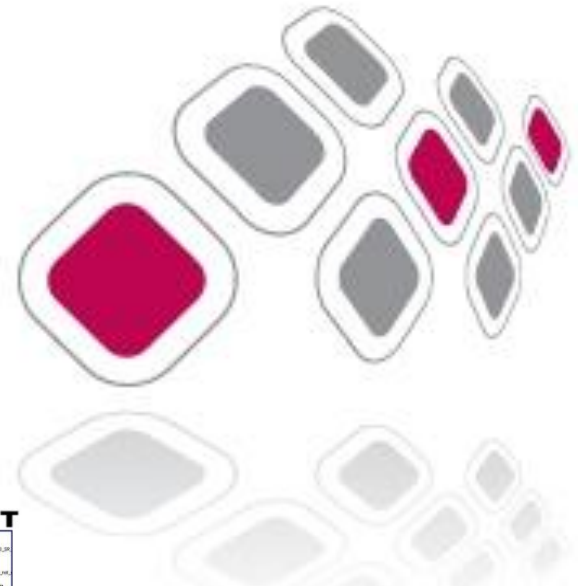
## HVLED available on eDesignSuite

[www.st.com/edesignsuite](http://www.st.com/edesignsuite)





# WEB Support





[www.st.com/edesign](http://www.st.com/edesign)

## eDesignSuite

The smart tool to design your application

Power Supply  
DC/DC - AC/DC



LED Lighting  
DC/DC - AC/DC



Photovoltaic  
DC/DC



Battery Charger  
AC/DC



Login to  
[www.st.com/edesignsuite](http://www.st.com/edesignsuite)  
(online registering is required)

OR

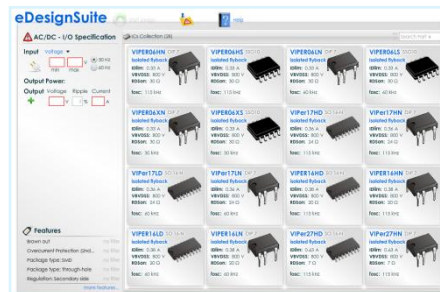
Fill in  
eDesignSuite Widget  
(visit Viper\*\* product pages  
on [www.st.com](http://www.st.com))

OR

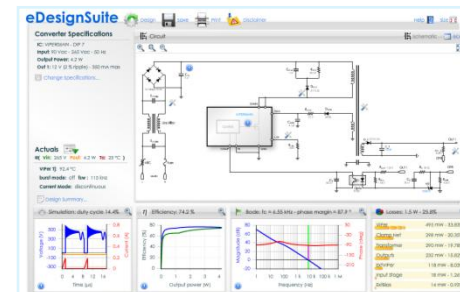
Open  
eDesignSuite off-line version  
(ask to ST Sales office to get  
it)



Choose Power Supply  
application type  
and create your design



Insert your I/O specifications and  
select one of the proposed Viper\*\*



The design is ready!



1

2

3

4

**A complete design in a few steps**



[www.st.com/edesign](http://www.st.com/edesign)

**eDesignSuite**

A full set of commands



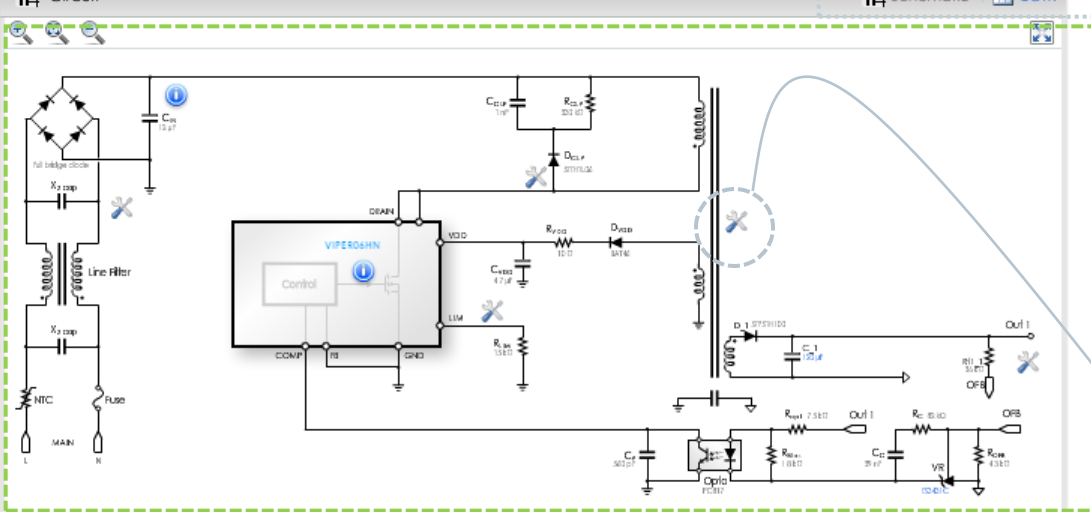
## Converter Specifications

IC: VIPER06HN - DIP 7  
Input: 90 Vac - 265 Vac - 50 Hz  
Output Power: 4.2 W  
Out 1: 12 V (2 % ripple) - 350 mA max  
[Change Specifications...](#)

## Actuals

@ ( Vin: 265 V Pout: 4.2 W Ta: 25 °C )  
VIPer Tj: 92.4 °C  
burst mode: off fsw: 115 kHz  
Current Mode: discontinuous  
[Design Summary...](#)

## Circuit



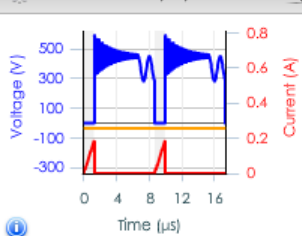
Help ? Size

Schematic BOM

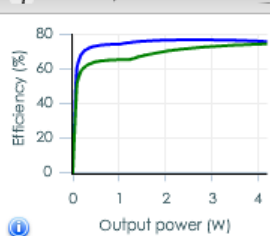
A fully and interactive BOM

A fully annotated and interactive schematic

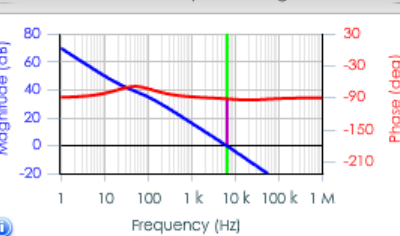
Simulation: duty cycle 14.4%



η Efficiency: 74.2%



Bode: fc = 6.55 kHz - phase margin = 87.9 °



Losses: 1.5 W - 25.8%

VIPer	495 mW - 33.83%
Clamp Net	298 mW - 20.35%
Transformer	290 mW - 19.78%
Outputs	232 mW - 15.82%
ExtVIPer	118 mW - 8.03%
Input Stage	18 mW - 1.26%
ExtBias	14 mW - 0.93%

The user can customize the Flyback transformer





# ***Thanks for your attention***

**Simone Franceschin – Silica FAEs**

[simone.franceschin@silica.com](mailto:simone.franceschin@silica.com)

