



### Current SLLIMM<sup>™</sup> portfolio

Up to	100W	in f	ree-air

#### SLLIMM-nano

- Dishwashers
- Refrigerators
- Fans & pumps, ...



#### SLLIMM

· Washing machine

• Air-conditioner

• Dryer, .....

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#### From 500W to 2.5kW



PN	I <sub>C</sub> (@ 25°C) [A]	Package	NTC	Bootstrap Diode	Rth [ºC/w]	Std input driving
STGIPN3H60A	3	NDIP-26L	No	Yes	50*	STGIPN3H60AT
STGIPN3H60	3	NDIP-26L	No	Yes	50*	STGIPN3H60(T)-H
STGIPS10K60A	10	SDIP-25L	Yes	Yes	3.8	
STGIPS10K60T	10	SDIP-25L	Yes	Yes	3.8	STGIPS10K60T-H
STGIPS10C60	10	SDIP-25L	Yes	Yes	3.8	STGIPS10C60(T)-H
STGIPS14K60	14	SDIP-25L	No	Yes	3.0	
STGIPS14K60T	14	SDIP-25L	Yes	Yes	3.0	STGIPS14K60T-H
STGIPL14K60	15	SDIP-38L	Yes	Yes	2.8	
STGIPS15C60	15	SDIP-25L	Yes	Yes	3.0	STGIPS15C60(T)-H
STGIPS20K60	18	SDIP-25L	No	Yes	2.4	
STGIPS20C60	20	SDIP-25L	No	Yes	2.7	STGIPS20C60(T)-H
STGIPL20K60	20	SDIP-38L	Yes	Yes	2.2	
STGIPS30C60	30	SDIP-25L	No	Yes	2.4	STGIPS30C60(T)-H
STGIPL30C60	30	SDIP-25L	No	Yes	2.2	

\* Value referred to Junction- ambient

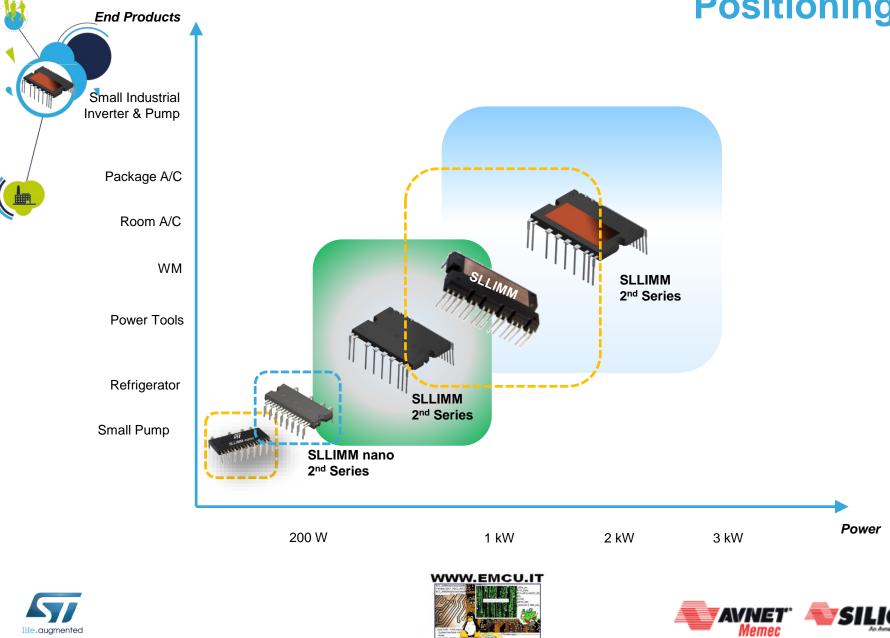


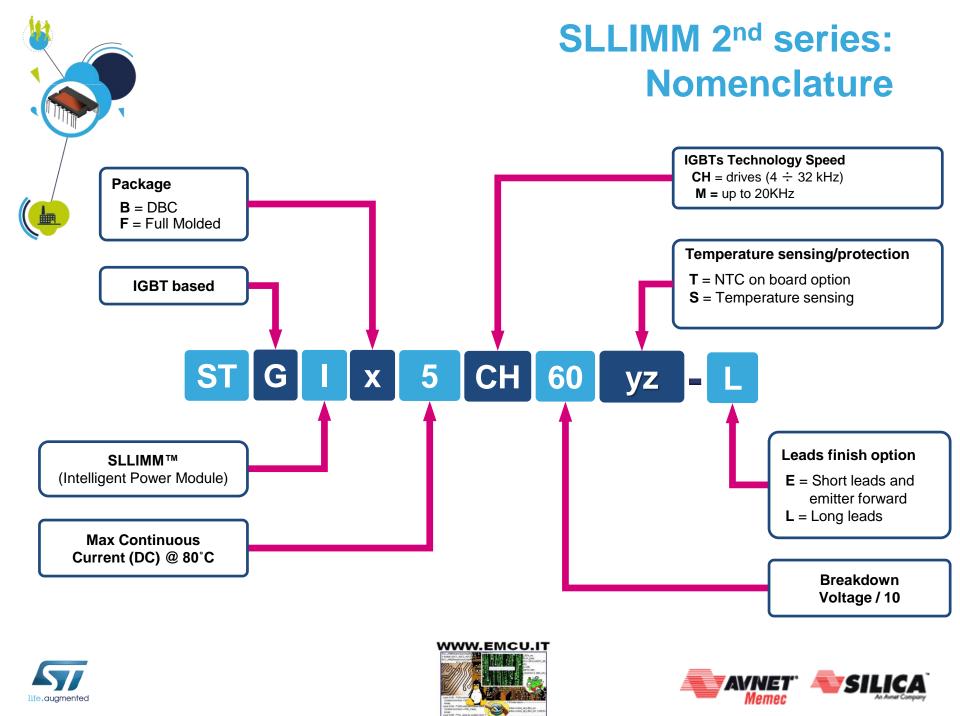


#### Main Customer using ST IPMs



### SLLIMM Series: Positioning







#### SLLIMM 2<sup>nd</sup> series: introduction 7

The SLLIMM series, small low-loss intelligent molded module family of intelligent power modules combine IGBT power switches in a 3-phase IGBT inverter stage configuration with freewheeling diodes, control Ics for gate driving, protections and other optional features in a single package, replacing more than 10 discrete devices.

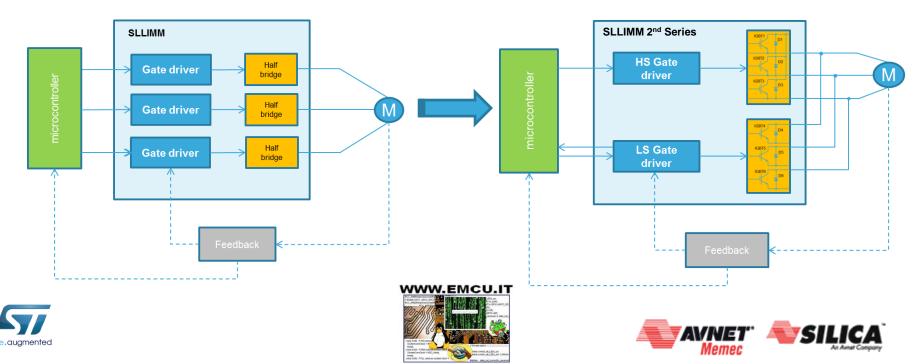
The SLLIMM 2<sup>nd</sup> series has been designed using a new internal configuration with only two drivers, one high side driver and one Low side driver.

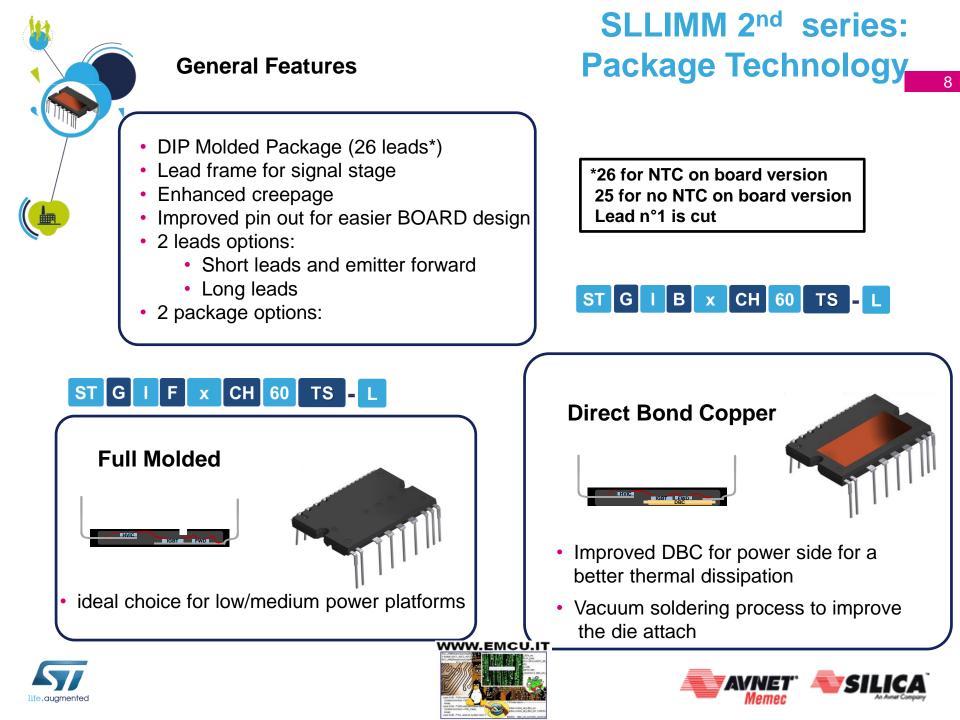
This new approach allows a more compact package and new advanced protection functions, thanks to the new features showed by Low side driver.

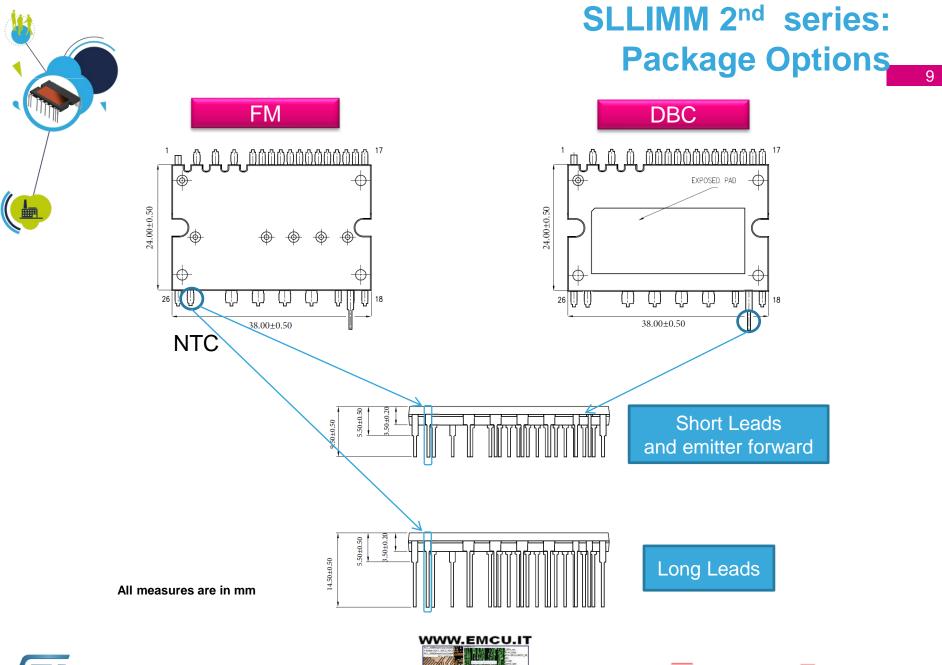
Two IPM versions are available, the Full Molded and the DBC (Direct Bond Copper) both compatible each other.

The products belonging to the new SLLIMM 2<sup>nd</sup> series show the best compromise between conduction and switching energy with an outstanding robustness and EMI behavior, making the new product ideal to enhance the efficiency of compressor, pumps, fans and low power motors working up to 20 kHz in hard-switching circuitries.

This series will complement and overcome the already available SLLIMM series in term of features, packages' types and flexibility.



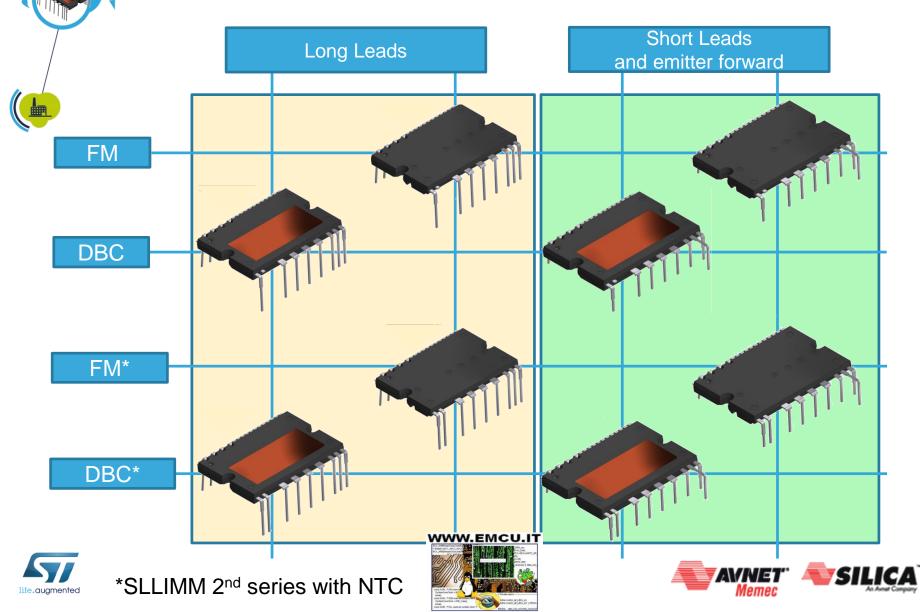


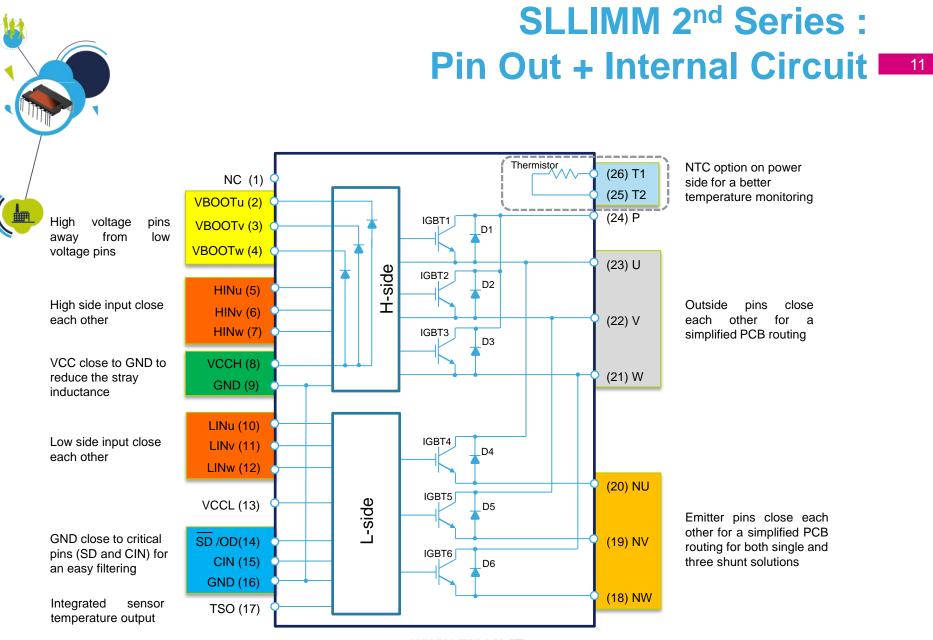






### **SLLIMM 2<sup>nd</sup> Series :** Package options <sup>10</sup>











### SLLIMM 2<sup>nd</sup> series: Product Features 12

FM/DBC fully isolated packages

cover a bigger range of power requirement

Integrated Bootstrap diode

Reduce BOM and simplified layout

Smart shut down

High speed fault condition info for the MCU to shut down internally the Nside IGBTs

**NTC thermistor** 

Temperature monitoring placed on the power side





Fault protections: over current

UVLO

Sense comparator

and short-circuit

**Thermal Sensor Output** 

Temperature sensor integrated to monitoring on the low side section

**Malfunctioning and fault prevention** 

for Vcc and Vboot



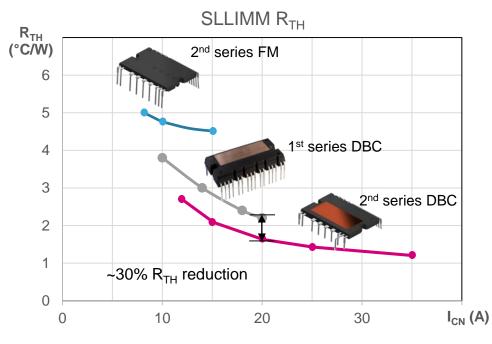




### SLLIMM 2<sup>nd</sup> Series: IGBT R<sub>TH(J-C)</sub> curves <sup>13</sup>

#### $2^{nd}$ series $Rth_{(j-c)}$ simulated values

PN	SLLIMM series		I <sub>CN</sub> @ 25°С	R <sub>TH(J-C)</sub> IGBT		
STGIF5CH60x	2 <sup>nd</sup>		8A	5.0 °C/W		
STGIF7CH60x		FM	10A	4.8 °C/W		
STGIF10CH60x			15A	4.6 °C/W		
STGIB8CH60x		2nd	2nd		12A	2.9 °C/W
STGIB10CH60x			15A	2.1 °C/W		
STGIB15CH60x				DBC	20A	1.7 °C/W
STGIB20CH60x					25A	1.45 °C/W
STGIB30CH60x			35A	1.25 °C/W		
STGIPS10K60			10A	3.8 °C/W		
STGIPS14K60		DBC	14A	3 °C/W		
STGIPS20K60	1 <sup>st</sup>	DBC	18A	2.4 °C/W		
STGIPL20K60			20A	2.2 °C/W		



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### SLLIMM 2<sup>nd</sup> Series: Synoptic table

Package	Part Number	lc @ 25°C (@ 80°C)	Voltage	Vce(sat) @ 25°C	Rthj-c (max)	Viso	Max T <sub>J</sub>	Samples (Mass Prod)
	STGIF5CH60TS-L(E)	8A (5A)	600V	1.6V	5.0 °C/W	1500V	175°C	Done
	STGIF7CH60TS-L(E)	10A (7A)	600V	1.6V	4.8 °C/W	1500V	175°C	wk 29 (wk30)
SDIP2F-26L	STGIF10CH60TS-L(E)	15A (10A)	600V	1.6V	4.6 °C/W	1500V	175°C	wk 30 (wk31)
	STGIB8CH60TS-L(E)	12A (8A)	600V	1.6V	2.9 °C/W	1500V	175°C	wk 33 (Q3 '15)
	STGIB10CH60TS-L(E)	15A (10A)	600V	1.6V	2.1 °C/W	1500V	175°C	wk 31 (wk32 )
	STGIB15CH60TS-L(E)	20A (15A)	600V	1.6V	1.7 °C/W	1500V	175°C	wk 31 (wk 32)
	STGIB20M60TS-L(E)	25A (20A)	600V	1.6V	1.45 °C/W	1500V	175°C	wk 33 (Q4 '15)
SDIP2B-26L	STGIB30M60TS-L(E)	35A (30A)	600V	1.6V	1.25 °C/W	1500V	175°C	wk 33 (Q4 '15)





#### Temperature sensing/protection

- T = NTC on board
- **S** = Temperature sensing

Leads finish option

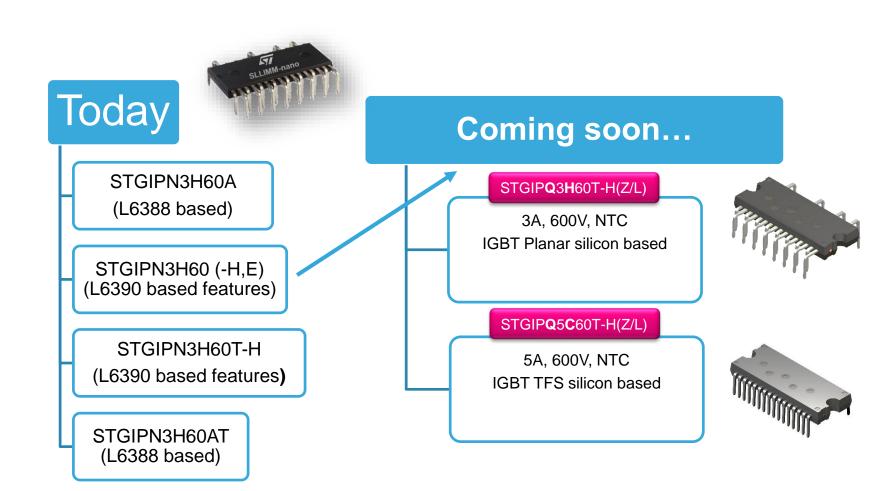
- E = Short leads and emitter forward
- L = Long leads







### SLLIMM-nano: Overview











#### SLLIMM nano series: introduction 16

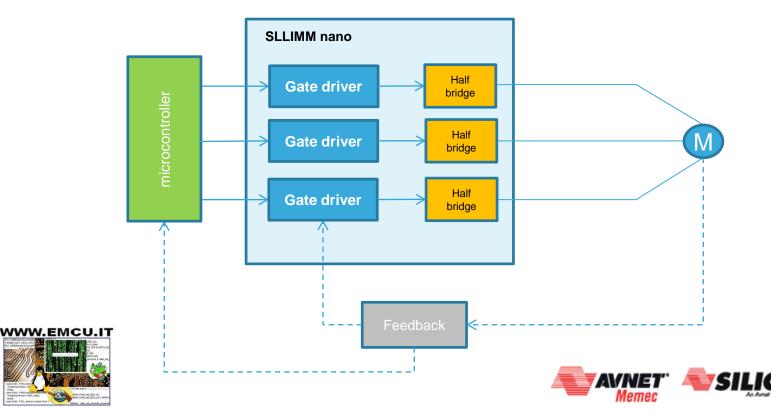
The **SLLIMM nano** has been designed using an internal structure of the inverter stage that includes three half-bridge HVICs for gate driving and six IGBTs with freewheeling diodes.

In add to the first series of this product a new series has been introduced, the new series shows a new package solution with mounted slots to allow a better and easy screw on heatsink.

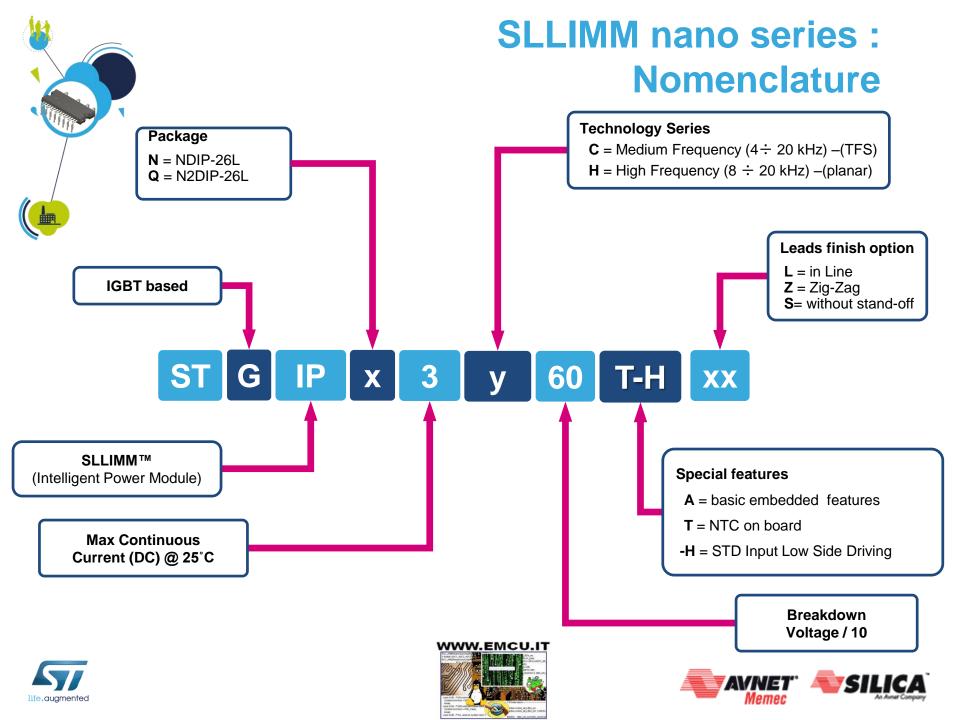
In add the in line version and the option with and without stand-off leads' packages are available.

The package is optimized for thermal performance and compactness in built-in motor applications, or other low power applications where assembly space is limited.

SLLIMM nano products show the best compromise between conduction and switching energy with an outstanding robustness and EMI behavior, making the product ideal to enhance the efficiency of compressor, pumps, fans and low power motors working up to 20 kHz in hard-switching circuitries.

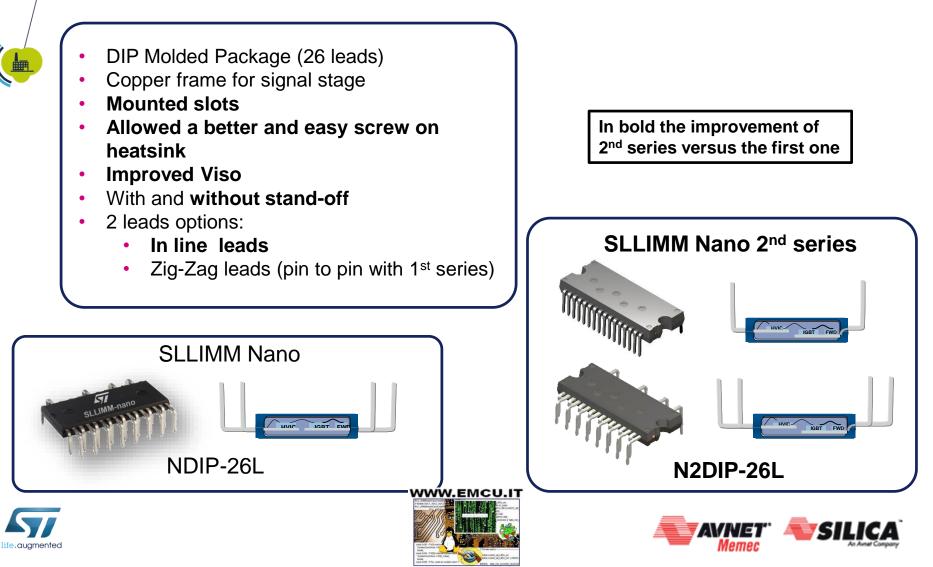


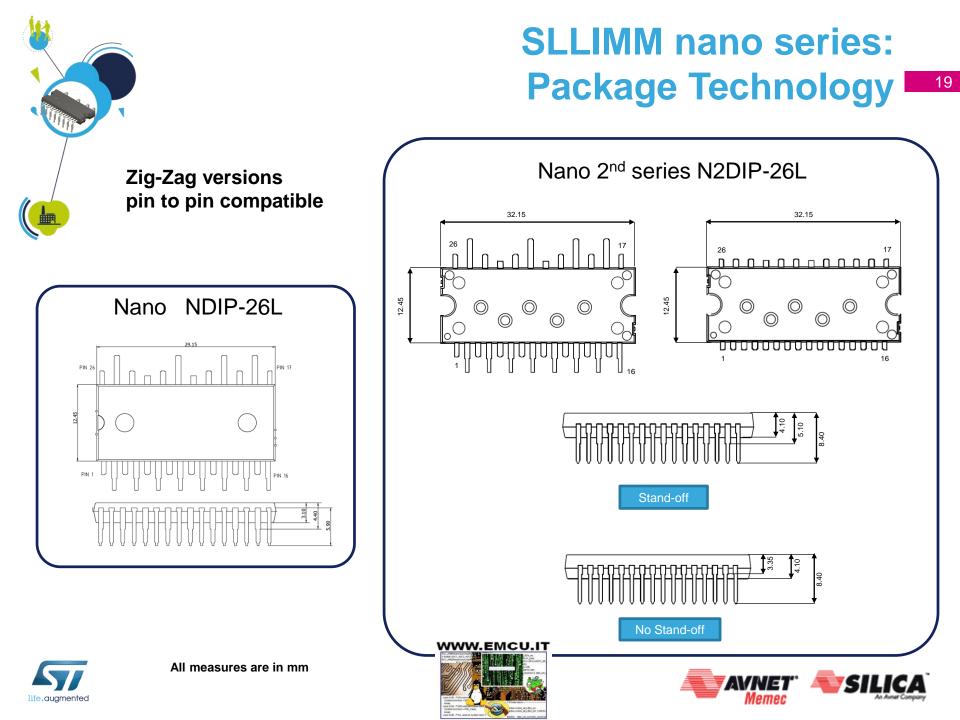


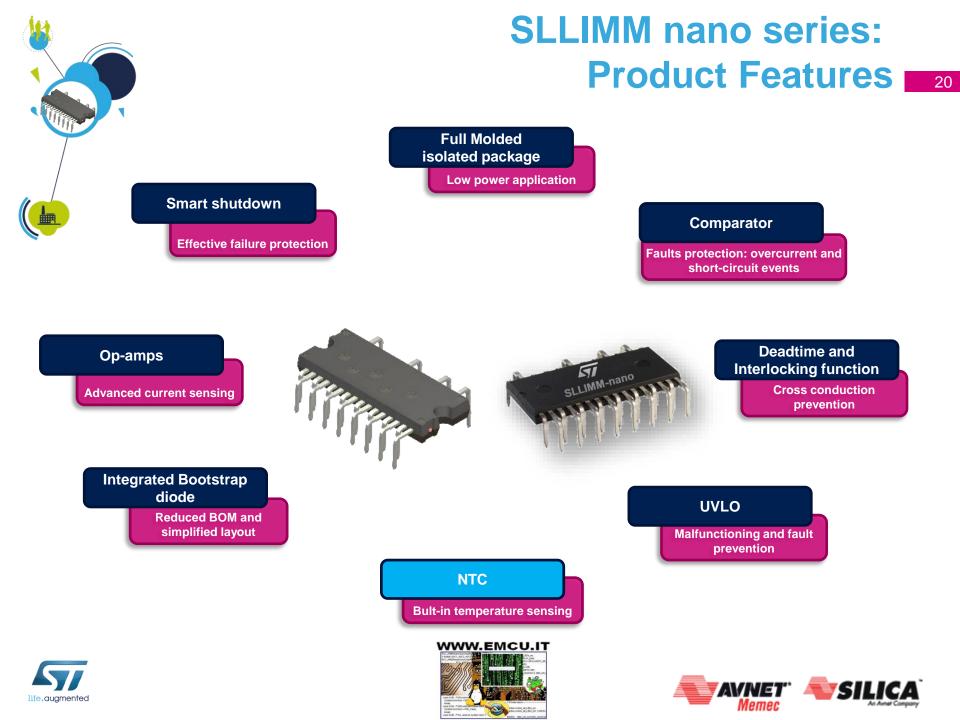




#### **General Features**







# **SLLIMM** nano: Synoptic table

Package	Part number	lc @ 25°C	Vcesat	Voltage	Viso	Samples (Mass Prod)
STI SLLIMM-nano	STGIPN3H60A(T)	3A	2.15V	600V	1000V	DONE
SLLIMM-nano	STGIPN3H60 (-H,E)	3A	2.15V	600V	1000V	DONE
NDIP-26L	STGIPN3H60T-H	3A	2.15V	600V	1000V	DONE
EFFER STATE	STGIPQ3H60T-HZ(S)	3A	2.15V	600V	1500V	Done(wk30)
	STGIPQ3H60T-HL(S)	3A	2.15V	600V	1500V	Done(wk30)
	STGIPQ5C60T-HZ(S)	5A	1.65V	600V	1500V	Done(wk30)
N2DIP-26L	STGIPQ5C60T-HZ(S)	5A	1.65V	600V	1500V	Done(wk30)

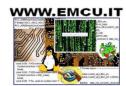
**T** = NTC on board

-H = STD Input Low Side Driving

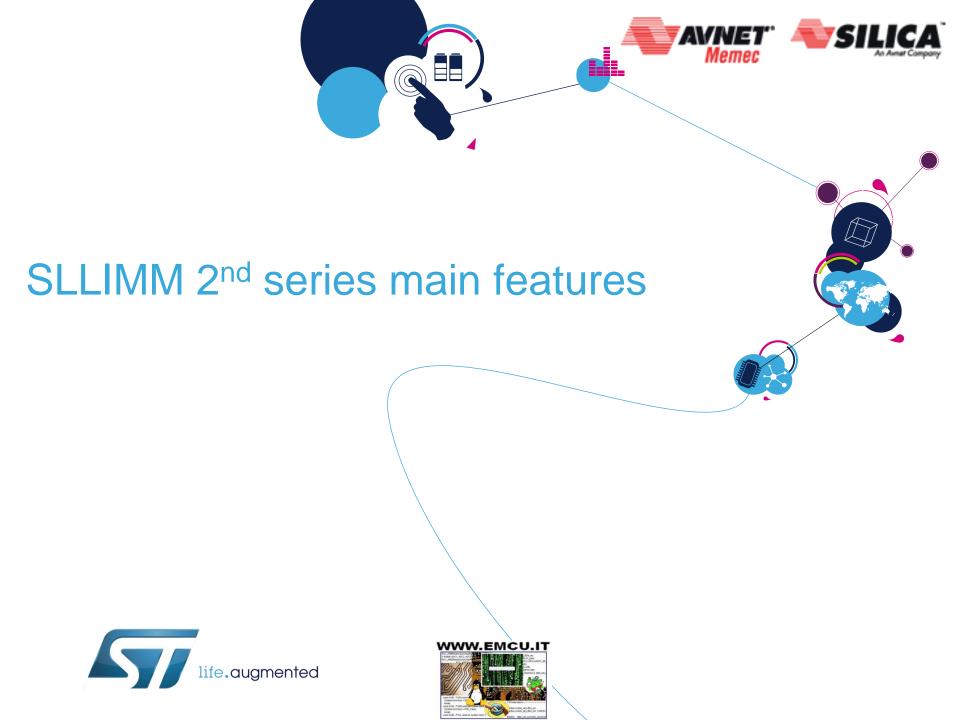
-E = ESD protection on board

Leads finish option Z =zig zag leads L = in line S= without stand-off option









# Main Features Summary 23

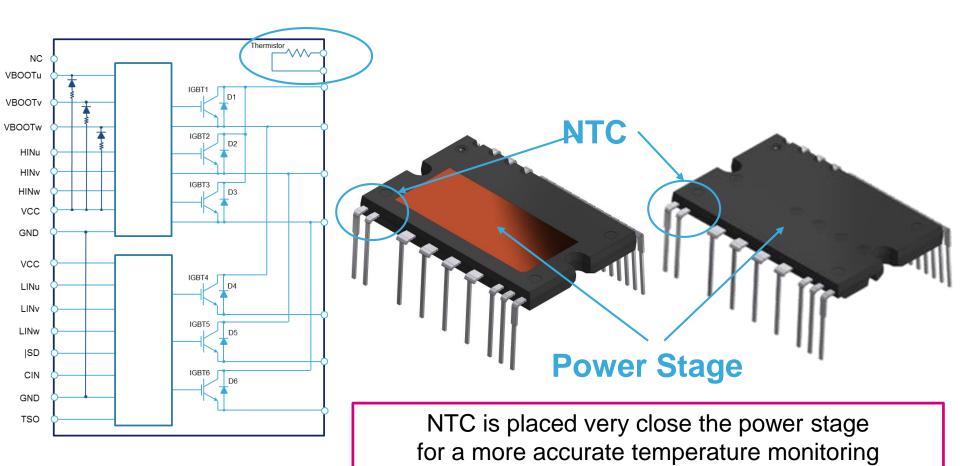
- NTC Thermistor
- Thermal sensor output
- Bootstrap Section
- Shutdown, Smart SD
- Internal Comparator
- UVLO Protection



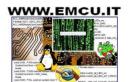




# SLLIMM<sup>™</sup> Gen 2: NTC Thermistor 24

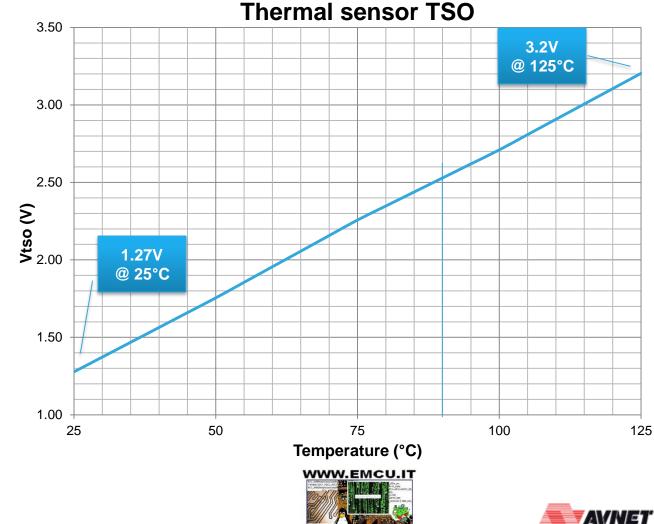








# Thermal Sensor Output 25

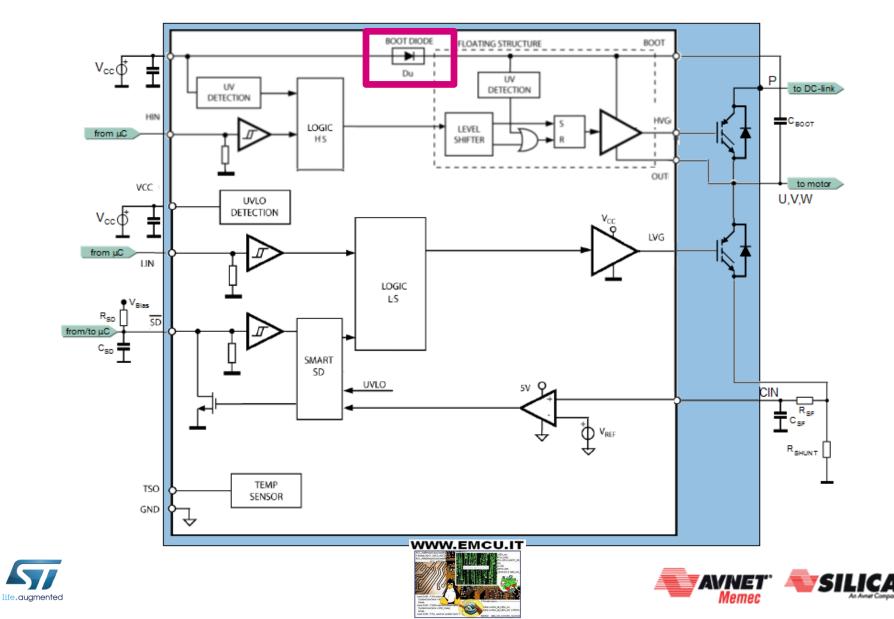


#### SLLIMM 2<sup>nd</sup> series



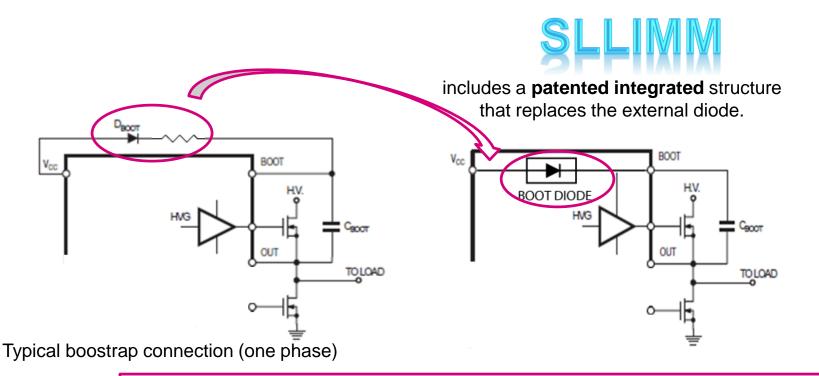


# Bootstrap Block Diagram 26



# Bootstrap Section 27

The easiest way to supply the high voltage section of the IPM is to realize a floating bootstrap power supply. This function is normally accomplished by a high voltage fast recovery diode plus a small series resistor.



Less passive components on the PCB board: easy layout

Higher integration level means less assembly step  $\rightarrow$  HIGHER RELIABILITY

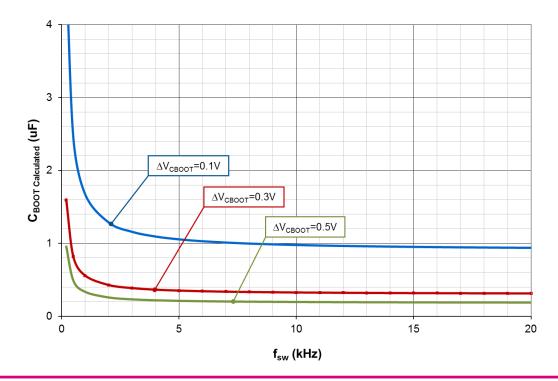






# Suggested value for bootstrap capacitor

In order to help customer during the design phase, **S7** will provide the <u>suggested</u> bootstrap capacitors values for a given conditions.



- Continuous sinusoidal modulation
- Duty cycle  $\delta = 50\%$
- $V_{CC} = 16.5V$
- Can be used as a worst case for all the SLLIMM IPM

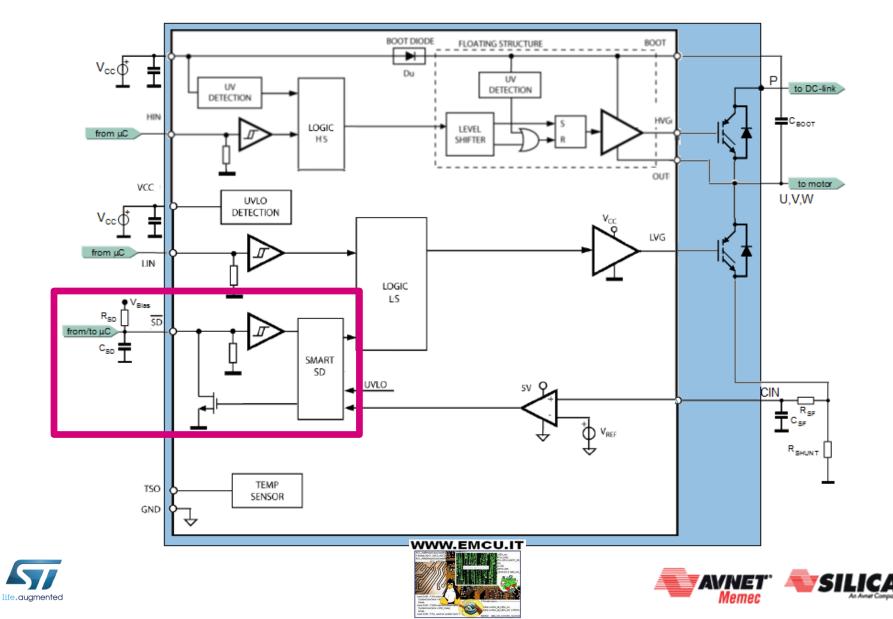
Considering the limit cases during the PWM control and further leakages and dispersions in the board layout, the capacitance value to use in the bootstrap circuit must be selected two or three times higher than the CBOOT calculated in the above graph.







# Shutdown Block Diagram 30



# Shutdown Function (SD) 31

/SD-OD is an **input-output pin**.

It can be used by the microcontroller to rapidly shutdown the SLLIMM (see below truth table) or can be used by the SLLIMM to inform the microcontroller that a fault condition occurred.

#### /SD function truth table

Condition		Inputs	Outputs		
	SD	LINX	HINx	LVGx	HVGx
Shutdown enable half-bridge tri-state	L	х	х	L	L
0 "logic state" half-bridge tri-state	н	L	L	L	L
1"logic state" low side direct driving	н	н	L	н	L
1"logic state" high side direct driving	н	L	н	L	н

Note: X: don't care

Whatever are the input signals, if the SD function is activated (active low) the output signals are always OFF



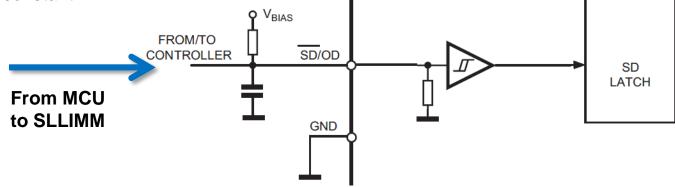




# Shutdown Function (SD) 32

#### Shutdown signal from MCU

Just connect the /SD pin to the MCU with a simple pull-up resistors. Add an RC block to fix the re-enable time constant.



To properly size the RC block please consider that you must ensure that the proper voltage level is maintained to enable/disable the SLLIMM. Please refers to the following table:

Symbol	Parameter	Min	Тур	Max
VIL	Low logic level voltage			0.8V
VIH	High logic level voltage	2.25V		

To enable SLLIMM by MCU -> VSD > VIH(min) To disable SLLIMM by MCU -> VSD < VIL(max)

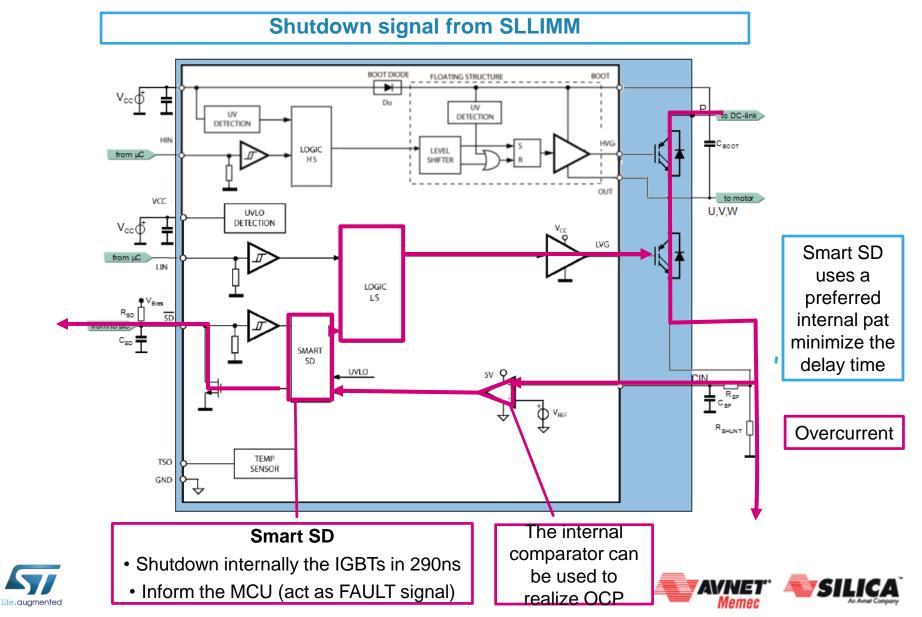




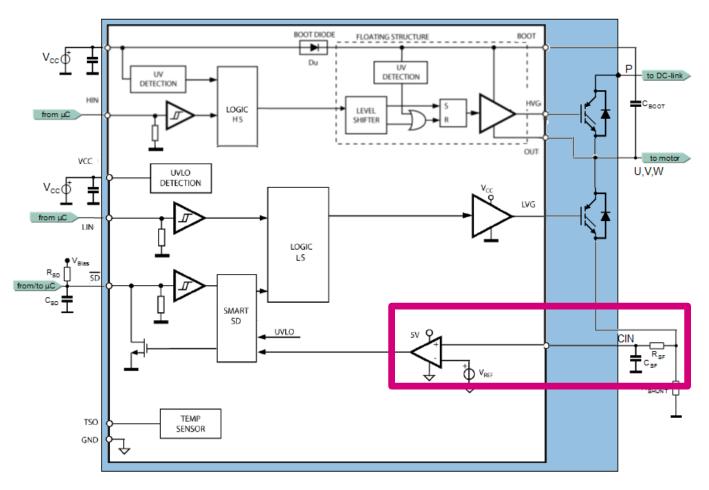




# Shutdown Function (SD) 33



# Comparator Block Diagram 34

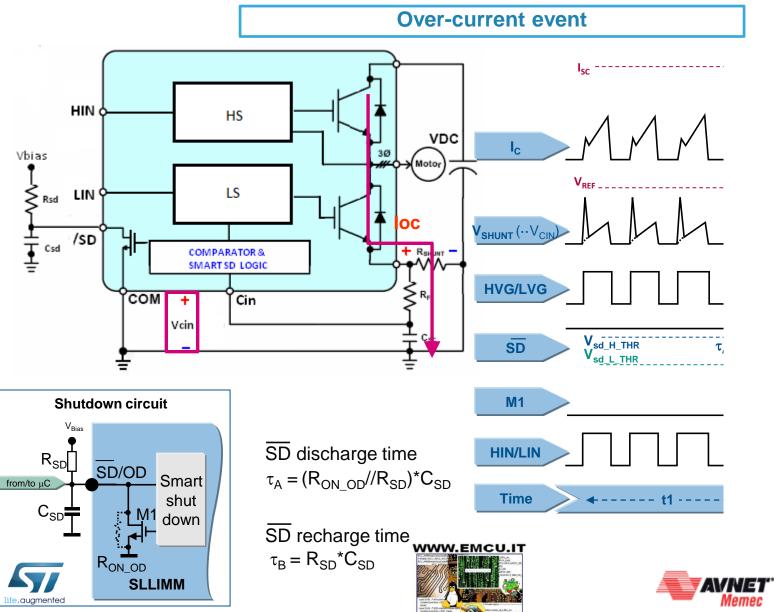








### Comparator and Smart Shutdown (SSD) 35



# Fault signals 36

### SLLIMM 2ND SERIES

Symbol	Parameter	Event time	SD open-drain enable time result
00	OC Over-current event	≤ 20 µs	20 µs
Over-current event	≥ 20µs	OC time	
	≤ 50 µs	50µs	
UVLO	Under-voltage lock out event	≥ 50µs until the VCC exceed the VCC UV turn ON threshold	UVLO time

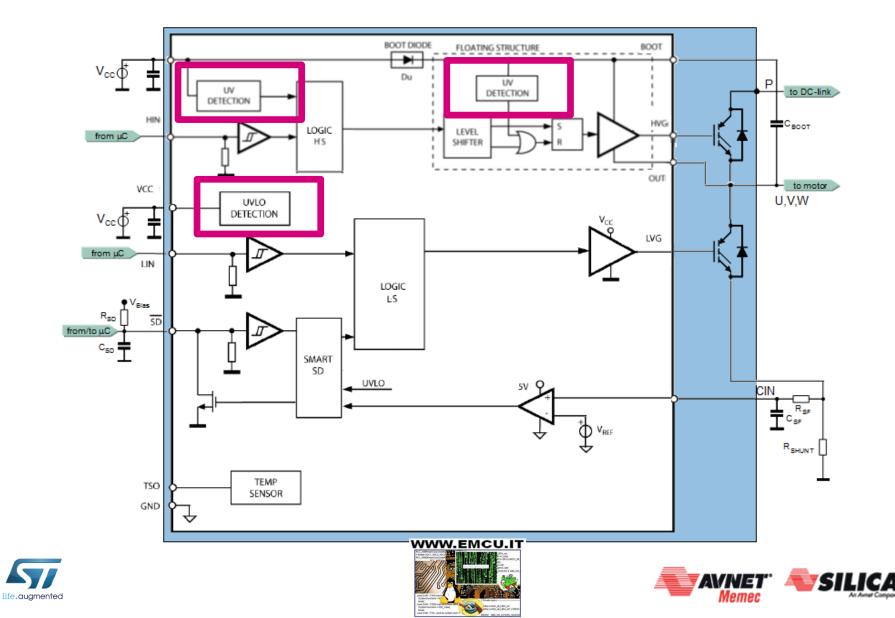
Fault timings								
t <sub>oc</sub>	Overcurrent fault time	Full Temperature range	14	20	26	μs		
t <sub>uvlo</sub>	UVLO fault time	Full Temperature range	35	50	<mark>6</mark> 5	μs		





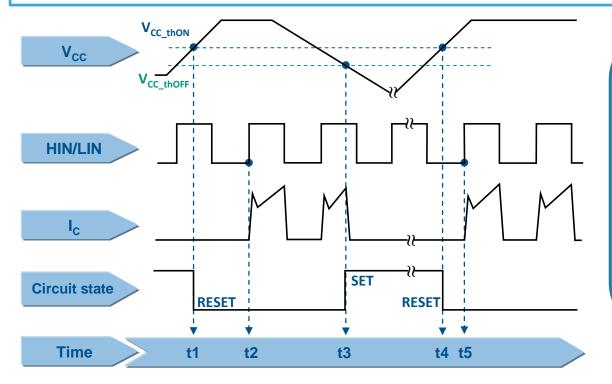


# UVLO Block Diagram 37



#### Undervoltage Lockout Function (UVLO)

**UVLO**: If Vcc or Vboot voltages go below the UVLO\_thOFF, the driver is shut down to avoid any high-power-dissipation condition for the IGBT or improper functioning of SLLIMM.

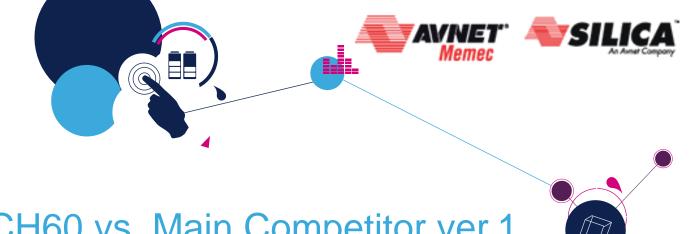


- t1: VCC>VCC\_thON the SLLIMM starts
- t2: HIN/LIN is on and the IGBT is turned on
- t3: VCC<VCC\_thOFF the UVLO event is detected. The IGBT is turned off
- t4: VCC>VCC\_thON the SLLIMM re-starts
- t5: HIN/LIN is on and the IGBT is turned on again









#### ST STGIF5CH60 vs. Main Competitor ver.1, Main Competitor ver.2







# Synoptic Table 40

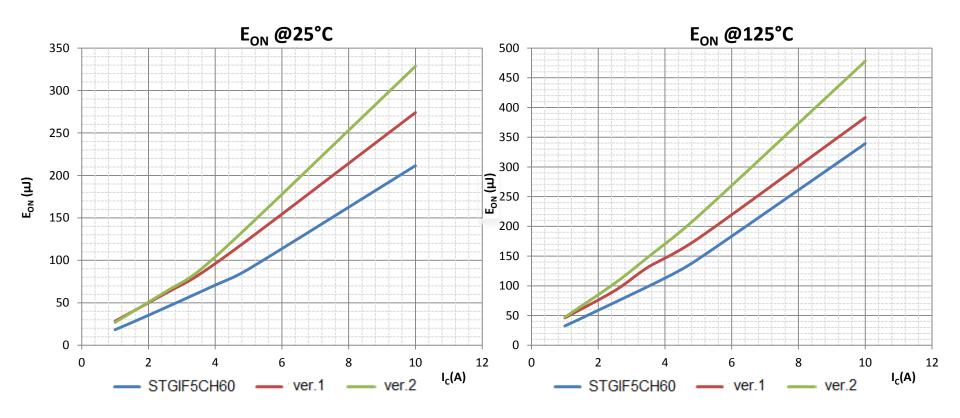
Device	STGIF5CH60TS-E T - NTC on board S - integrated temperature sensor E - (short leads), L (long leads)	Main Competitor ver.1	Main Competitor ver.2
Voltage (V)	600	600	600
Current @ $T_c = 25^{\circ}C$ (A)	8	5	5
$R_{th(j-c)}$ max single IGBT (°C/W)	5.0	4,7	5
Package type	SDIP2F-26L FULL MOLDED	DBC	DBC
Number of pin	26 (NTC on board optional) 25	25	25
Package size (mm) X, Y, Z	38.0x24.0x3.5	38.0x24.0x3.5	38.0x24.0x3.5
Integrated bootstrap diode	Yes	Yes	Yes
SD/FAULT function	Yes	Yes	Yes
Comparator for fault protection	Yes (1 pin)	Yes (1 pin)	Yes (1 pin)
Smart shutdown function	Yes	No	No
Protection	Under voltage protection (UV) Short circuit protection (SC) Over temperature protection (OT) (optional)	Under voltage protection (UV) Short circuit protection (SC) Over temperature protection (OT) (optional)	Under voltage protection (UV) Short circuit protection (SC) Over temperature protection (OT) (optional)
Fault event monitoring	UV - SC - OT (optional) different timing feedback per event	UV – SC no differentiations per event	UV – SC no differentiations per event
Temperature monitoring	Temperature sensor NTC sensor on board (optional)	Temperature sensor (optional)	Temperature sensor (optional)
Undervoltage lockout	Yes	Yes	Yes
Open Emitter configuration	Yes (3 pins)	Yes (3 pins)	Yes (3 pins)
Emitter forward	(short lead type) STGIF5CH60xy-E	short lead type	short lead type







# Dynamic Comparison: IGBT E<sub>ON</sub>



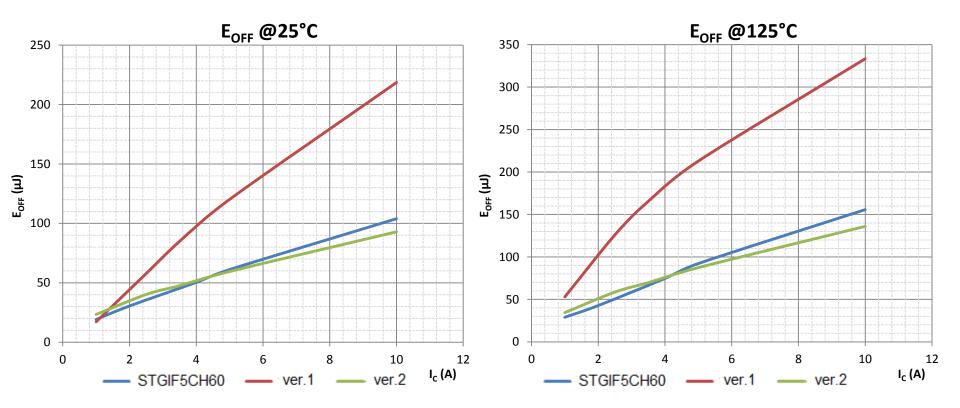
STGIF5CH60 shows better dynamic performance, during the ON phase, in all the range of current and in both junction temperatures.







## Dynamic Comparison: IGBT E<sub>OFF</sub> 42



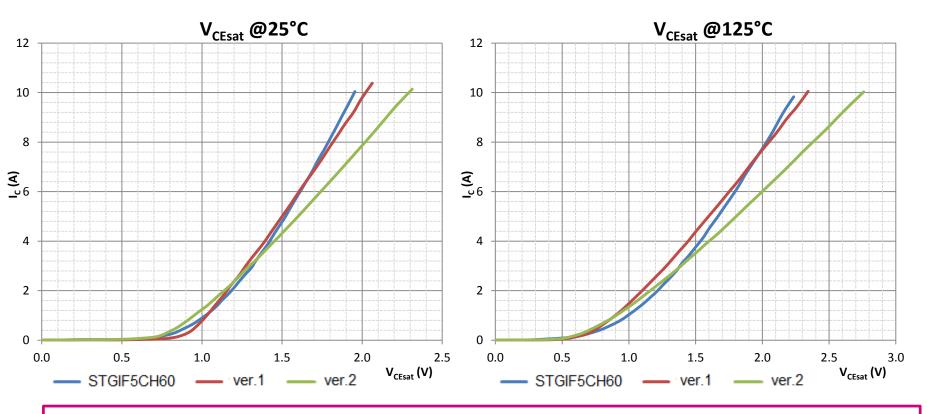
STGIF5CH60 shows a much better dynamic performance, during the ON phase, in all the range of current and in both junction temperatures compared to Main Competitor ver.1. Comparable behavior with Main Competitor ver.2.







## Static Comparison: IGBT V<sub>CE sat</sub> I



STGIF5CH60 vs. Main Competitor ver.1: similar behavior @25°C, slightly worse @125°C (up to 3.5 A). STGIF5CH60 vs. Main Competitor ver.2: slightly worse behavior in both conditions of junction temperature (up to 3.5 A).

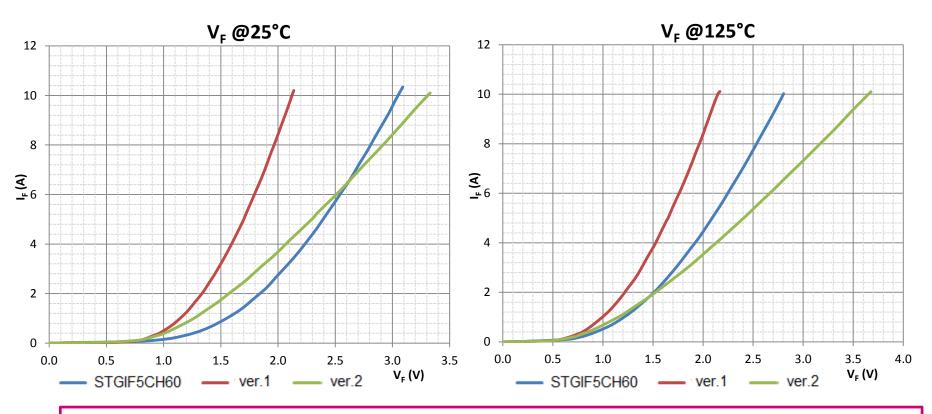






43

## Static Comparison: FW diode V<sub>F</sub>



STGIF5CH60 vs. Main Competitor ver.1: has a worse behavior in term of forward voltage of antiparallel diode in both conditions of junction temperature. STGIF5CH60 vs. Main Competitor ver.2: worse behavior @25°C and similar or better @125°C.







# Simulation Parameters 45

- V<sub>bus</sub>= 300V
- ma= 0.8
- PF= 0.6
- $f_{sine} = 60Hz$
- $f_{sw}$  = up to 20kHz
- I<sub>peak</sub>= 3.5 A
- V<sub>CEsat</sub>, V<sub>F</sub>= typical values <u>measured</u> @ 25°C & 125°C
- E<sub>ON</sub>, E<sub>OFF</sub>= typical values <u>measured</u> @ 25°C & 125°C
- Gate driving conditions= internal, due to IPM configuration

#### **Total power loss were evaluated**





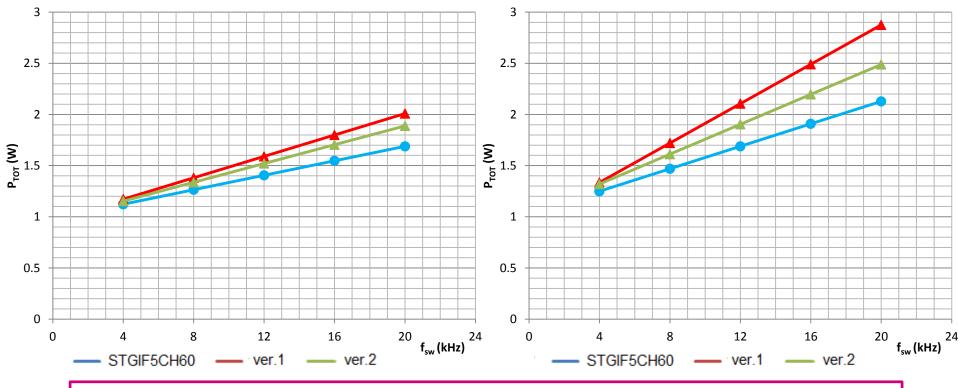




#### IGBT Total Power Loss @3.5A

Ipeak= 3.5 A, Tj= 25 °C

Ipeak= 3.5 A, Tj= 125 °C



Single IGBT of STGIF5CH60 has a better efficiency in both junction temperature conditions and in all the range of frequency under analysis, than competitors.







# Thermal simulation 47

The thermal behavior of the devices under comparison was analyzed considering the following test conditions:

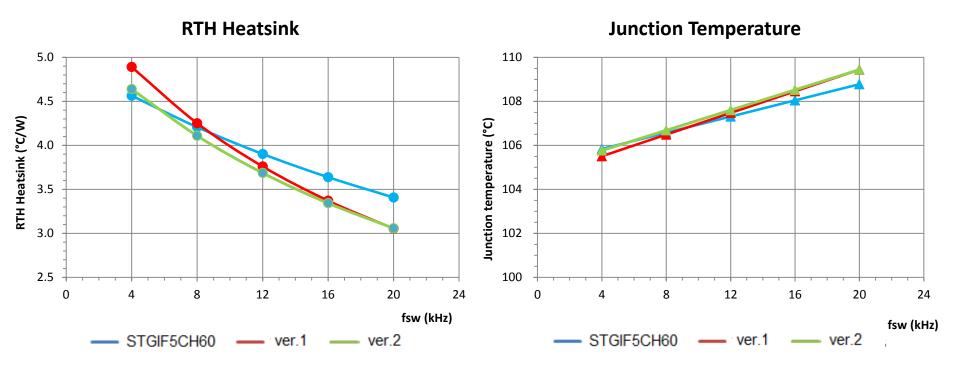
T<sub>case</sub> fixed @100°C: assuming the same case temperature (T<sub>c</sub>=100°C), ambient temperature (Ta=50°C) and current (Ipeak=3.5A) the thermal resistance of the required heatsink and the junction temperature were calculated.







#### Test 1: T<sub>case</sub> fixed @100°C



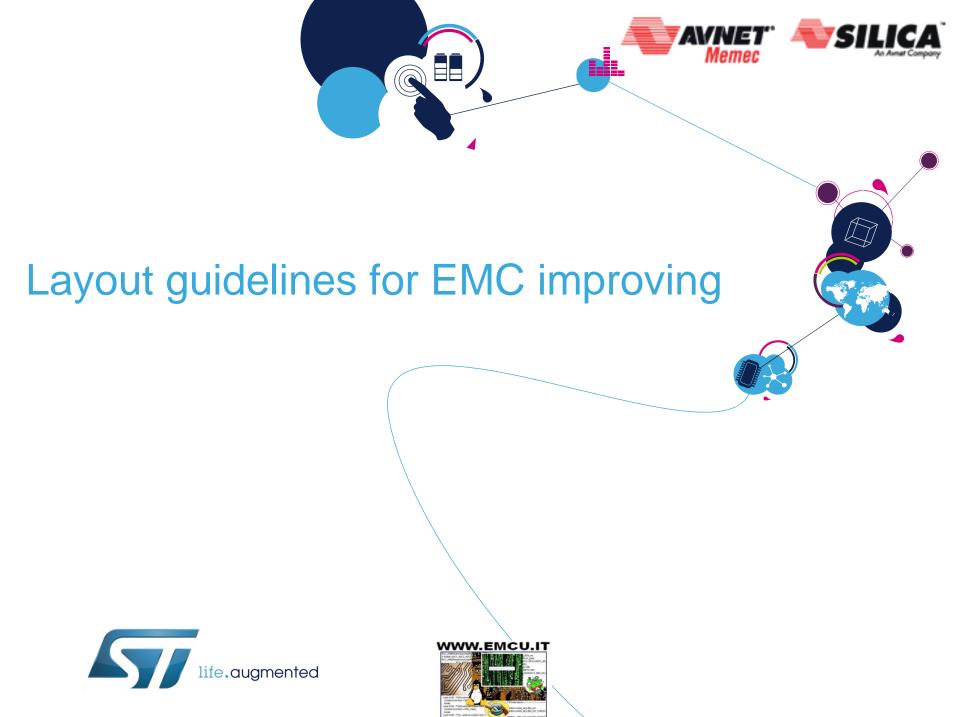
In order to keep the same case temperature ( $T_c=100^{\circ}C$ ), STGIF5CH60 requires a smaller heatsink than Main Competitor ver.2, in almost all the range of switching frequencies. Compared to Main Competitor ver.1 it requires a smallest heatsink starting from about 8kHz. This allows smaller size and lower costs solutions (thanks to the lower power dissipation).

No particular differences in terms of junction temperatures.



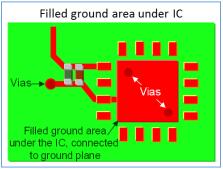






#### Ground 50

- separate signal ground tracks from power ground tracks and connect with at a single star connection directly on the shunt resistors
- wide ground traces reduce parasitic inductance
- fill unused board spaces with copper areas connected to the ground plane, especially underneath all the high frequency IC



- when more than one power supply is required, separate the power and ground tracks
- when a multilayer PCB is used, implement a complete ground layer or place ground traces in parallel with power traces to keep the supply clean

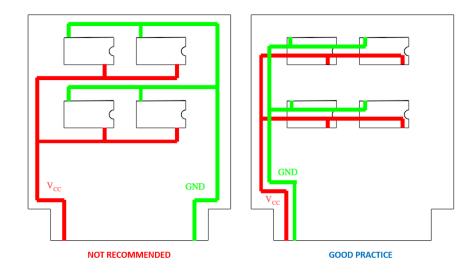






#### Power 1/3 51

 route parallel to ground on the same or adjacent layers to minimize loop area wide ground traces reduce parasitic inductance



- PCB planes or wide traces reduce parasitic inductance
- bypass capacitors (aluminum or tantalum) placed as close as possible to each IC and IPM reduce the transient circuit demand on the power supply

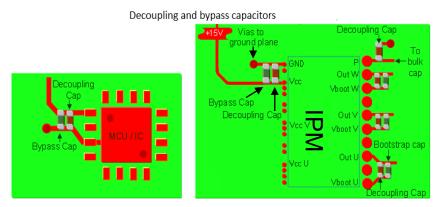






#### Power 2/3 52

decoupling capacitors (with low ESR) placed as close as possible in parallel with the bypass capacitor reduce high frequency switching noise on the power supply lines



- decoupling capacitors (with low ESR) placed as close as possible in parallel • with the bypass capacitor reduce high frequency switching noise on the power supply lines
- a 21 V Zener diode connected to each power supply pin prevents surge destruction









- a decoupling capacitor (with low ESR) in parallel with each bootstrap capacitor filters high frequency disturbances
- a 21V Zener diode in parallel with each bootstrap capacitor prevents surge destruction
- a decoupling capacitor (with low ESR) in parallel with the electrolytic bulk capacitor filters surge voltage; both capacitors should be placed as close as possible to the power device (the decoupling capacitor has priority over the bulk capacitor)
- use low inductance shunt resistors for phase leg current sensing
- minimize the wiring length between the shunt resistor and power ground to avoid malfunctions
- connect signal ground and power ground at only one point (near the terminal of the shunt resistor) to avoid any malfunction due to power ground fluctuation









- increase the distance between adjacent tracks and separate them to minimize capacitance coupling interference
- place sensitive and high frequency away from high noise power tracks
- on double-layers boards, place signal and power tracks on the same side and ground on the other
- do not use wire jumpers, minimize layer transitions for critical signal traces and keep the same number of vias on each signal track where necessary









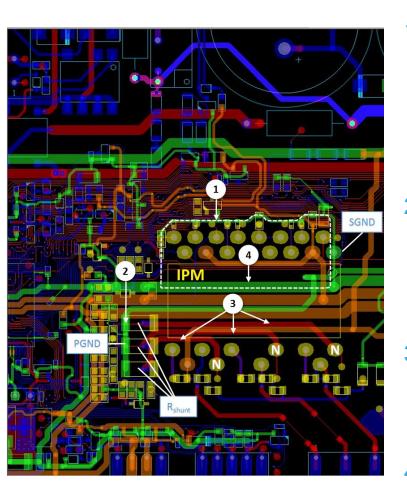
- group components according to their functionality (analog, digital, power, lowspeed and high-speed sections)
- place a filter at subsystem boundaries to promote signal flow between different sections
- minimize the number of vias, especially in the high frequency signal tracks, as they introduce parasitic impedance; distribute them around the PCB, avoiding concentrations in small areas
- prefer star connections to stub connections, especially on critical signal tracks, as the latter produces reflections
- keep a constant signal track width during the entire routing as variations change its impedance and produce reflections
- unused pins cannot be unconnected and must be pulled-up or pulled-down
- respect current flow in layout design in EMI input filters











#### Expample 1 57

- ground tracks form a closed loop (white dashed line) which may increase EMC problems by introducing noise into the ground (due to high voltage switching tracks) and affect driver or application performance
- the signal ground (SGND) of the IPM is connected away from the power ground (PGND); all signal grounds must be connected in a star configuration to the power ground
- the shunt resistors are too far from the N-pins of the IPM and connected asymmetrically (the net lengths are too dissimilar)
  - power ground tracks are too narrow; this may increase parasitic inductance

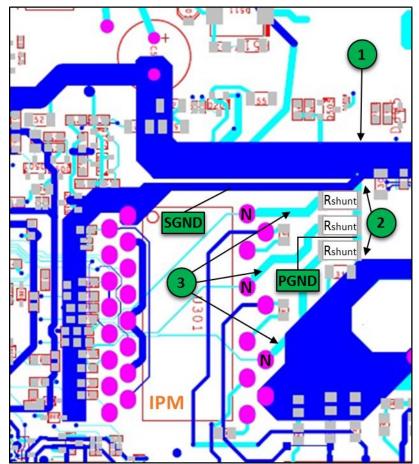




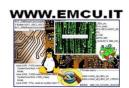


# Expample 1, improving

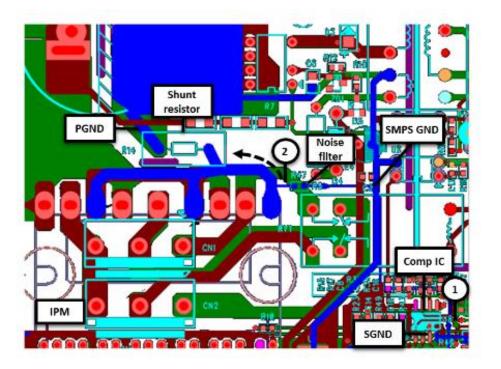
- the ground path has been reshaped to remove any loops and increase the width/length ratio of the tracks
- 2. the shunt resistor ground has been changed to a star point configuration for both signal and power grounds
- the shunt resistors have been relocated to guarantee shorter and symmetric connections with the N pins of the IPM







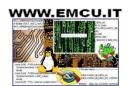




## Expample 2 59

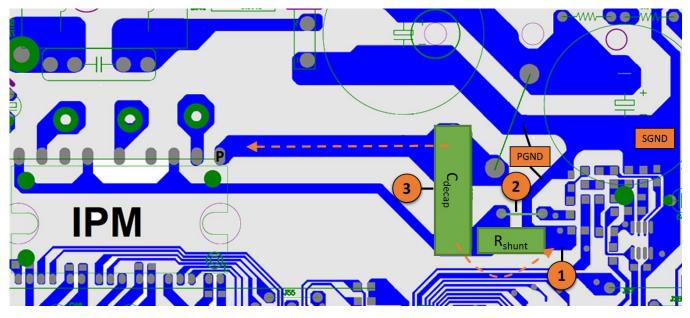
- the comparator ground for OCP (SGND) is too far from shunt resistor R14 (PGND) and it crosses the SMPS power supply ground; finally, the comparator IC should be closer to the shunt resistor and away from noisy tracks
- the current sensing track should be connected directly to shunt resistor R14 and the filtering capacitor must be placed as close as possible to the comparator pin to reduce the level of noise that could trigger false overcurrent protection







## Expample 3 60



- 1. separate the signal ground tracks from the power ground tracks and connect them at a single point by using the shunt resistors in a star configuration; widen the power ground track
- 2. jumpers on current sensing tracks should be avoided; the RC filter ground must be connected to the IC comparator ground
- the decoupling capacitor on the bus voltage should be connected between the P pin of the IPM (as close as possible) and the power ground (on the shunt resistor)





